

Phantom-Less Nonlinear Magnetic Resonance Imaging Calibration With Multiple Input Blood Flow Model

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Abstract: Purpose: Previous work used phantoms to calibrate the nonlinear relationship between the gadolinium contrast concentration and the intensity of the magnetic resonance imaging signal. This work proposes a new nonlinear calibration procedure without phantoms and considers the variation of contrast agent mass minimum combined with the multiple input blood flow system. This also proposes a new single-input method with meaningful variables that is not influenced by reperfusion or noise generated by aliasing. The reperfusion in the lung is usually neglected and is not considered by the indicator dilution method. However, in cases of lung cancer, reperfusion cannot be neglected. A new multiple input method is formulated, and the contribution of the pulmonary artery and bronchial artery to lung perfusion can be considered and evaluated separately.

Methods: The calibration procedure applies the minimum variation of contrast agent mass in 3 different regions: (1) pulmonary artery, (2) left atrium, and (3) aorta. It was compared with four dimensional computerized tomography with iodine, which has a very high proportional relationship between contrast agent concentration and signal intensity.

Results: Nonlinear calibration was performed without phantoms, and it is in the range of phantom calibration. It successfully separated the contributions of the pulmonary and bronchial arteries. The proposed multiple input method was verified in 6 subjects with lung cancer, and perfusion from the bronchial artery, rich in oxygen, was identified as very high in the cancer region.

Conclusions: Nonlinear calibration of the contrast agent without phantoms is possible. Separate contributions of the pulmonary artery and aorta can be determined.

Key Words: 4D MRI perfusion, calibration, Gd contrast agent, multiple input model, reperfusion

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Informed consent was obtained from all individual participants included in this study.

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Hemodynamic and perfusion analyses are currently performed by injecting an intravenous bolus with gadolinium (Gd), and the lung is imaged using 4D magnetic resonance imaging (MRI) with the signal variation observed at the input (blood vessels) and at the output (lung tissue). However, 2 problems remain to be solved: (1) contrast calibration and (2) blood reperfusion.

Quantification of the Gd tracer concentration is an essential step and needs to be determined at each point to allow hemodynamic analysis. A simplification procedure assumes that the change in signal intensity or relative signal intensity because of the tracer is directly proportional to the tracer concentration.^{1,2} However, the effect of nonlinearity is particularly large in areas of high concentration,³ such as the input position in perfusion analysis, and any input component may be overestimated. The proposed is a calibration procedure using phantoms, which works even for high concentrations of the contrast agent, or regions where the contrast characteristic reverses.⁴ Some issues of the proposed method were found. When a high-concentration contrast agent was injected into the patient, the image quality was reduced and some artifacts occurred. The phantoms deteriorate over time, and it was necessary to use new phantoms for each imaging procedure. These issues motivated us to propose a nonlinear calibration method based on the minimum variation of the mass of the contrast agent, which does not require phantoms.

The pulmonary arteries leave the heart and carry deoxygenated blood to the lungs. After oxygenation of the blood, the blood leaves the lungs and returns to the heart. Most of the oxygenated blood goes to the body, and a small part enters the lungs to keep them alive. This phenomenon will be called lung reperfusion. Lung reperfusion is generally considered to be approximately 1%⁵ of the whole blood flow (BF) and is neglected by conventional methods.^{1,6} However, lung reperfusion increases and cannot be neglected in cases of lung cancer.⁷ The multiple input model proposed here considers lung reperfusion and its applications for analyzing lung cancer and performing functional and nutritional vasculature analysis separately. Although 2-input perfusion has been proposed in the past,⁸ they used the maximum slope method, which assumes rapid intravenous injection of a contrast agent, and depending on the patient's condition, this is not true. The multiple-input analysis method proposed here has characteristics that do not depend on the input waveform.

MATERIALS AND METHODS

Calibration of Gd Tracer Concentration and Signal Intensity in MRI

In this work, lower levels of Gd tracer concentration are used, and the proposed tracer calibration procedure does not require any phantom. Figure 1 presents the route of the blood with Gd. The Gd concentrations in the pulmonary artery, left atrium, and aorta are represented as $C_{art}(t)$, $C_{la}(t)$, and $C_{aor}(t)$. The BF term is the blood flow in that vessel, and the M term is the total mass of the contrast tracer in the first perfusion of that vessel.

Initially, contrast blood enters the right heart through the vena cava and pumps to the lungs through the pulmonary artery with BF. Blood is oxygenated in the lungs and goes to the left atrium through the pulmonary vein. This oxygenated blood has 3 routes: aorta, coronary artery, and bronchial artery. Most goes to the entire body through the aorta, but some of it goes back to the lungs through the bronchial artery. The remainder goes to the heart through the coronary artery.

Now, blood from the bronchial artery becomes deoxygenated after passing through the lungs, and there are 2 possible routes: the bronchial and pulmonary veins. Blood that goes through the pulmonary veins to the left heart has a small portion of deoxygenated blood (lung shunt) combined with oxygenated blood. Based on this discussion, $C_{art}(t)$ is the first input of blood to the lungs and $C_{aor}(t)$ is the second input.

Note that there are 3 circulatory pathways. The first is a circulatory path going through the pulmonary artery and has BF. This circulatory path will be called circulatory path of pulmonary artery (CP-PA). The second is a circulatory path with BF equal to $l \times BF$ and represents the pulmonary shunt. This circulatory path will be called circulatory path of pulmonary shunt (CP-PS). The third is a circulatory path going through the coronary artery and has BF equal to $n \times BF$. This circulatory path will be called CP-CA.

Considering exclusively CP-PS, after infinite iterations, the amount of contrast mass that passes through the left atrium can be determined by

$$M + \frac{l}{1+l}M + \left(\frac{l}{1+l}\right)^2 M + \dots = \sum_{n=0}^{\infty} M \left(\frac{l}{1+l}\right)^n = (1+l)M. \quad (1)$$

Because the BF in the left atrium is $(1+l)BF$, the amount of contrast going through the left atrium is as follows:

$$(1+l)M = (1+l)BF \int_0^{\infty} C_{la}(t)dt \quad (2)$$

$$M = BF \int_0^{\infty} C_{la}(t)dt$$

The aorta undergoes a similar procedure (considering exclusively CP-PS), resulting in

$$(1-m-n)M = (1-m-n)BF \int_0^{\infty} C_{aor}(t)dt \quad (3)$$

$$M = BF \int_0^{\infty} C_{aor}(t)dt$$

A similar procedure can be applied to the bronchial artery. From the above, the integration of $C(t)$ in time is constant, independent of the part, and can be written as

$$\int_0^{\infty} C(t)dt = \frac{M}{BF} \quad (4)$$

Eq. (4) is also valid for the pulmonary artery as all contrast passes through it. This result considers an ideal world, where no errors occur. In the real world, it is necessary to deal with errors and the variation of the integration of $C(t)$ in time is considered minimum.

In this research, the contrast concentration used is low and preserves a nonlinear and monotonic relationship with the intensity of the MRI signal. Therefore, we propose a calibration using

$$C(t) = \alpha \left\{ \exp \left[\beta \left(\frac{SI(t)}{SI(0)} - 1 \right) \right] - 1 \right\} \quad (5)$$

The values of α and β are determined by minimizing the tracer concentration in the following compartments: the pulmonary artery, the aorta, and the left atrium. Minimization is solved by the Levenberg-Marquardt method. The function to be minimized is

$$\arg \min_{\alpha, \beta} = \left(\int C_{aor} - \int C_{art} \right)^2 + \left(\int C_{la} - \int C_{art} \right)^2 \quad (6)$$

Hemodynamic Analysis

Theory

The indicator dilution method was established as a theory for hemodynamic analysis,^{9,10} and each voxel can be used to analyze a section and determine regional blood volume (rBV; mL_{Blood}/mL_{Voxel}), regional mean transit time (rMTT; s) and regional blood flow (rBF; mL_{Blood}/mL_{Voxel}/s).¹¹

$$rBV = \frac{\int_0^{\infty} C_{tis}(t)dt}{\int_0^{\infty} C_{art}(t)dt} \quad (7)$$

$$rMTT = \int_0^{\infty} h(t)tdt \quad (8)$$

$$rBF = \frac{rBV}{rMTT} \quad (9)$$

where $C_{tis}(t)$ is the average contrast concentration that occupies the tissue inside a voxel. $h(t)$ is the probability distribution function of the tracer transit time, and using the out-flow concentration $C_{out}(t)$, it is given by

$$h(t) = \frac{C_{out}(t)}{\int_0^{\infty} C_{out}(t)dt} \quad (10)$$

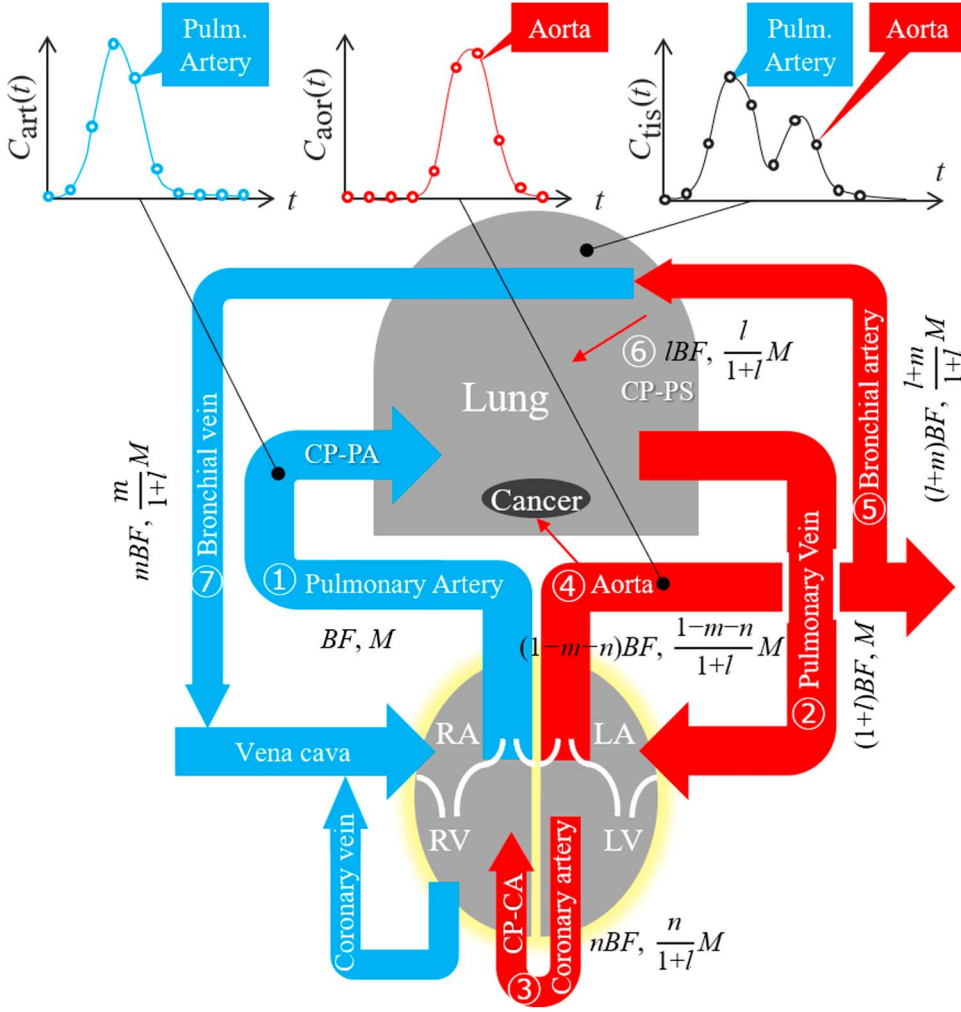


FIGURE 1: Schematic representation of the circulatory system is shown. Blood concentration in the pulmonary artery, aorta, and lungs is represented by graphs such as $C_{art}(t)$, $C_{aor}(t)$, and $C_{tis}(t)$.

Because outflow cannot be observed in voxels, the residue function of the contrast inside the voxel $R(t)$ is used instead.

$$R(t) = rBF \left[1 - \int_0^{\infty} h(\tau) d\tau \right] \quad (11)$$

$C_{tis}(t)$ can be evaluated from the convolution of the accumulated amount of the tracer inside the voxel, defined by

$$C_{tis}(t) [mmol/ml_{Blood}] = \int_0^t C_{in}(\tau) R(t - \tau) d\tau. \quad (12)$$

Because the impulse input is impractical, the $r(t)$ estimation must be performed using an inverse filter. The inverse filter is

sensitive to noise, so γ -variate function was fitted to the input and output waveforms.^{1,6} However, this ignores CP-PS.

$$\gamma(t) = a(t - b)^c \exp \left[-\frac{(t - b)}{d} \right] \quad (13)$$

Multiple Input Method

We used a γ -variate function Eq. (13) to model the impulse response, instead of fitting γ -variate functions to the input and output waveforms. Substituting Eq. (4) and (8) into expression Eq. (11), it is possible to obtain a new expression to $R(t)$ by

$$R(t) = rBF \left\{ 1 - \int_0^t \left[\frac{\gamma(\tau)}{\int_0^{\infty} \gamma(t) dt} \right] d\tau \right\} \quad (14)$$

Table 1 Equipment and Parameters, the Only Difference Among the Patients' Parameters Used is the TR

MRI Type	Achieva 1.5T A-Series (Philips)
Type of Gd contrast	Magnevist
Bolus administration	5 mL/seconds flush with saline
TE	0.796 ms
TR	2349 ms (A) 2677 ms (B-F)
FA	25°
Number of phase encoding steps	132
Protocol name	Perfusion SENSE
Gd relaxivity	2500 mL/sec/mmol
CT type	Aquilion ONE (TOSHIBA)
ECG triggering	Not used

Repetition time was different for patient A.

FA indicates flip angle; Gd, gadolinium; MRI, magnetic resonance imaging; TE, echo time; TR, repetition time.

The γ -variate function parameters that minimize the difference

$$\arg \min_{\{a,b,c,d\}} \sum_{t=0}^n [C_{tis_{obs}}(t) - C_{tis_{cal}}(t)]^2 \quad (15)$$

between the observed $C_{tis_{obs}}(t)$ and the calculated $C_{tis_{cal}}(t)$ values are obtained by using the Levenberg-Marquardt estimation.¹² $C_{tis_{cal}}(t)$ can be obtained from $C_{in}(t)$ and $R(t)$ from Eq. (12) and (14). This is an inverse problem, and the initial values influence the final solution. The formulation of the inverse problem can be greatly modified to incorporate meaningful variables from which good initial values can be obtained.

Instead of using the γ -variate function from Eq. (13), it is possible to use the incomplete Γ function and regularized upper incomplete Γ function (Q-function) defined by¹³

$$\Gamma(a, x) = \int_x^\infty t^{a-1} e^{-t} dt \quad (16)$$

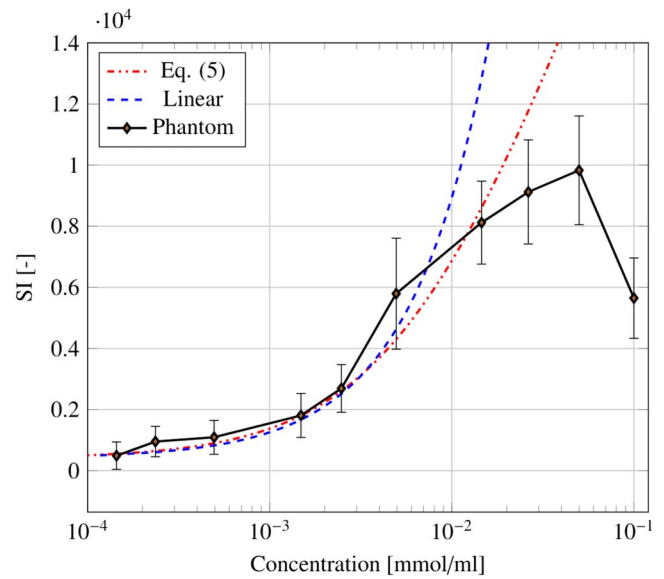
$$Q(a, x) = \frac{\Gamma(a, x)}{\Gamma(a)} \quad (17)$$

and after some algebraic manipulation, $r(t)$ can be represented by

$$R(t) = \begin{cases} rBF \times Q\left(\frac{\sigma^2}{d^2}, \frac{t - rMTT}{d} + \sigma^2\right), & t \geq rMTT \\ rBF, & \text{otherwise} \end{cases} \quad (18)$$

Table 2 Patient Characteristics

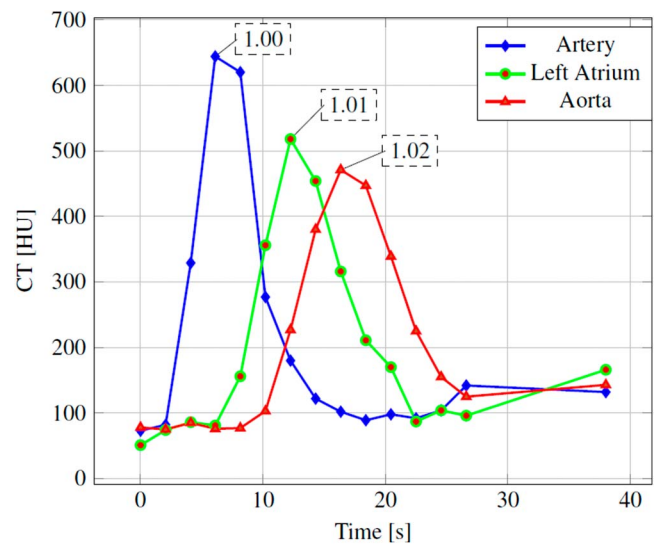
Patient	Sex	Disease
A	Male	Lung cancer
B	Male	Lung cancer
C	Male	Lung cancer
D	Male	Lung cancer
E	Male	Lung cancer
F	Female	Lung cancer

**FIGURE 2:** Comparison between the 3 calibration procedures: the conventional linear approximation, the one proposed in Eqn. 5, and the calibration using phantoms. Note that the horizontal axis is a logarithmic graph.

where

$$\sigma^2 = \int_0^\infty (t - rMTT)^2 h(t) dt = d^2(c + 1) \quad (19)$$

Expression Eq. (18) is the new single-input method with meaningful variables. When considering multiple inputs, we assign a subscript index to each input $C_{in,i}(t)$ and $R_i(t)$. $C_{tis_{cal}}$

**FIGURE 3:** Waveform of input and output observed by four dimensional computerized tomography (4D-CT). Inside each rectangle, the value of $\int C(t)dt$ is represented considering the pulmonary artery as a reference.

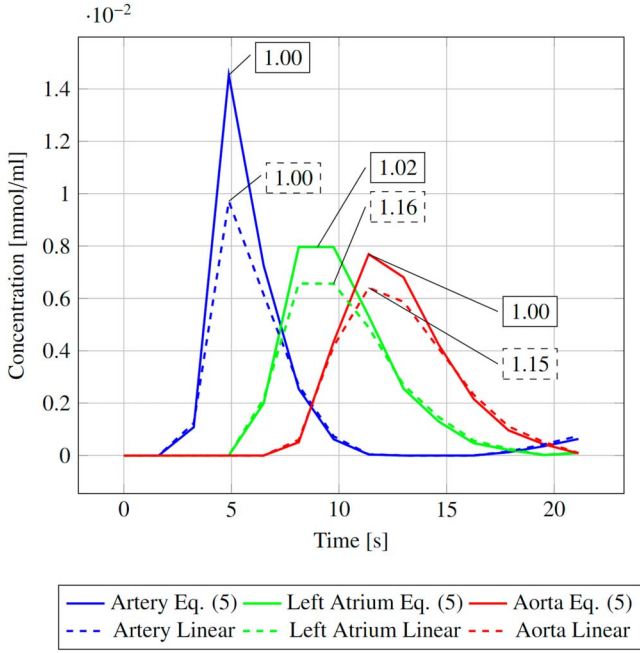


FIGURE 4: Results of the calibration showing the tracer concentration in the pulmonary artery, the left atrium, and the aorta. The value of $\int C(t)dt$ is represented inside each rectangle, considering the pulmonary artery as a reference.

expressed by Eq. (12), can be evaluated by accumulating $C_{in,i}(t)$ and $R_i(t)$, as

$$C_{tis_cal}(t) = \sum_i \int_0^t C_{in,i}(\tau) R_i(t - \tau) d\tau \quad (20)$$

Expressions Eq. (18) and (20) are used to minimize

$$\arg \min_{\{rBF_i, rMTT_i, \sigma_i, d_i\}} \sum_{t=0}^n [C_{tis_obs}(t) - C_{tis_cal}(t)]^2 \quad (21)$$

The initial values for rBF_i , $rMTT_i$ and σ_i can be obtained, and the convergence to an unintended local solution can be reduced. rBV can be determined with Eq. (9) where rBF and rMTT are already known.

The proposed method is not influenced by reperfusion or noise generated by aliasing. Therefore, it is possible to directly use the input and output waveforms without performing any curve fitting.

Table 3 Results for the Calibration Obtained for the 6 Patients Considering Eq. (5) and the Conventional Linear Calibration

Patients	Eq. (5)			Linear		
	Art	L Atr	Aor	Art	L Atr	Aor
A	1.00	1.02	1.00	1.00	1.16	1.15
B	1.00	1.09	1.01	1.00	1.16	1.11
C	1.00	1.16	0.94	1.00	1.21	1.14
D	1.00	1.01	0.99	1.00	1.06	1.03
E	1.00	1.00	1.00	1.00	1.07	1.04
F	1.00	1.04	0.98	1.00	1.10	1.12
Average	1.00	1.05	0.99	1.00	1.13	1.10

Experiment

The Spoiled Gradient Recalled Acquisition in Steady State (SPGR) method was used with a high-speed time series MRI of the chest (12 [slice], 12.0 [mm/slice], 1.62 [s/frame], 14 [frame], 256×256 [pixels], 1.68 [mm/pixels], coronal). Table 1 presents the device information and imaging parameters. The contrast agent Gd was adjusted to 0.05 mmol/kg according to the weight of the patient. The capture began concurrently with the subject holding his breath, and the contrast agent was injected immediately afterward. The analyses were performed exclusively on frames in the breath-hold state. The results shown here are related to 6 patients (see Table 2 for details).

Two calibration and BF analysis experiments were performed. In both experiments, the pulmonary artery, aorta, and left atrium were all specified as circles with a radius of 3 pixels. Then, the average signal intensity for each region was determined.

Calibration Experiment

The proposed calibration is compared with the conventional linear approximation and phantom calibration. In the phantom calibration,⁴ 11 contrast agent phantoms were placed near the subject's shoulder. Each phantom has a different value of Gd concentration, and its position and dimension in the image are known. The signal intensity associated with each phantom is determined by manually drawing a circle with a radius of 3 pixels. The associated pixel intensity average and standard deviation are determined for each phantom.

To validate the proposed calibration model represented by Eq. (5), we also compared it with four dimensional computerized tomography. The phantom study showed that the calibration of the iodine contrast concentration and the intensity of the CT signal present a high proportional relationship.¹⁴ The imaging conditions were (320 [slice], 0.5 [mm/slice], 2.05 [s/frame], 16 [frame], 512×512 [pixels], and 0.625 [mm/pixels]) of a healthy female subject.

Our BF Analysis

Multi-input BF analysis was performed to confirm the results of $C_{tis}(t)$ waveform optimization and to confirm the images analyzed.

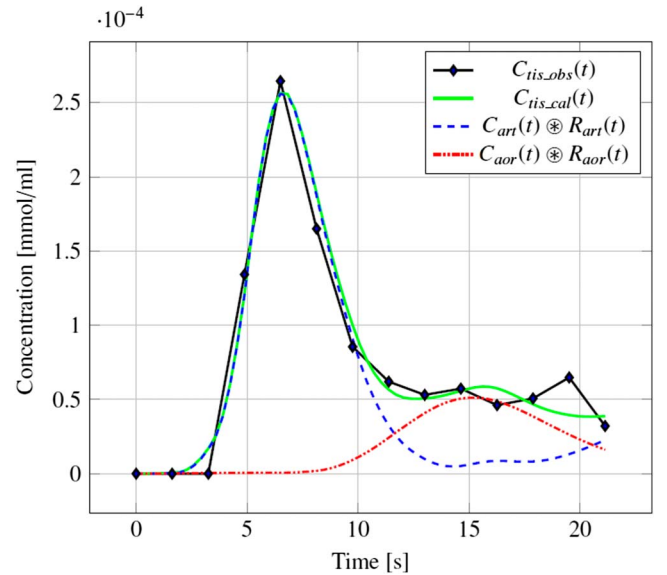


FIGURE 5: Result of the local analysis in the voxel inside the lung (patient A). The observed data are $C_{tis_obs}(t)$, and the calculated perfusion is $C_{tis_cal}(t)$. The contribution from the pulmonary artery is represented by $C_{art}(t) \otimes R_{art}(t)$. The contribution of the aorta is $C_{aor}(t) \otimes R_{aor}(t)$. \otimes means convolution.

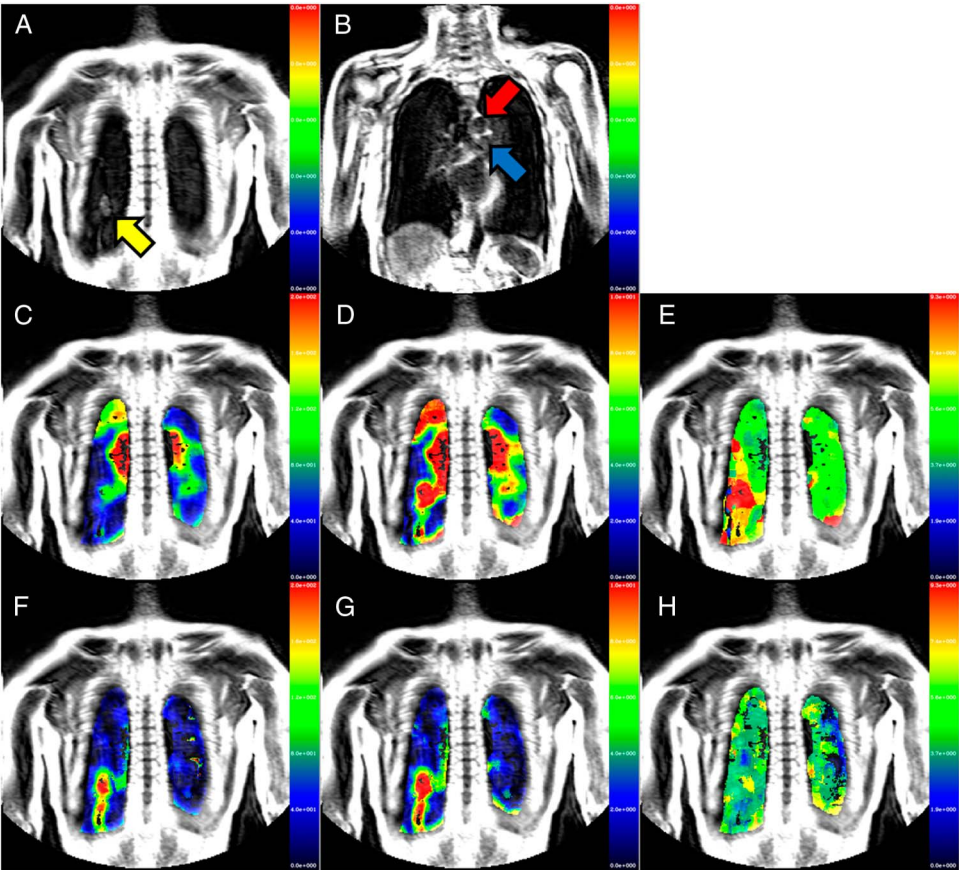


FIGURE 6: Results of the local analysis for lung perfusion. (A) Region of lung cancer shown by a yellow arrow. (B) The regions associated with the 2 inputs: pulmonary artery (blue arrow) and aorta (red arrow). (C) rBF_{art} . (D) rBV_{art} . (E) $rMTT_{art}$. (F) rBF_{aor} . (G) rBV_{aor} . (H) $rMTT_{aor}$.

The lung region is determined by the user manually. A percentile filter of the top 5% of signal intensity was used to remove the heart and some thick vessels. The initial values for rBF_i , $rMTT_i$ and σ_i are determined, and the Levenberg-Marquardt method is used to solve Eq. (21). A color mask shows the BF analysis results.

To evaluate the amount of CP-PS perfusion, the difference between the left and right cardiac output is calculated and compared. It is obtained using a Fast GE Cine. The diastolic and systolic areas of the right and left ventricles are segmented, and the difference between systolic output per stroke is calculated.¹⁵ The imaging parameters used are followed, and the epicardial and endocardial contours of the basal and apical slices were outlined manually.

Another approach to evaluate CP-PS is to integrate the rBV from each input contribution: pulmonary artery and aorta. Both the conventional linear approximation and the proposed calibration were performed, and $\int rBV_{art}$ and $\int rBV_{aor}$ were compared.

Table 4 Cardiac Output Using Fast GE Cine			
	Left Ventricle		Right Ventricle
Heart rate		81 bpm	
Stroke volume	54.4 mL		51.2 mL
Cardiac output	73.5 mL/s		69.2 mL/s
Difference left-right		4.3 mL/s	
CP-PS perfusion		6.2%	
The same subject with lung cancer is considered.			

RESULTS

Hemodynamic analysis Experiment

Figure 2 shows a comparison between the 3 calibration procedures: the conventional linear approximation, the calibration procedure defined by Eq. (5), and the phantom calibration. For pixels with higher intensity, the contrast concentration is underestimated by the conventional linear approximation compared with the one proposed here. Considering the phantom and linear calibrations, the linear model deviates from the phantom calibration at higher Gd concentrations up to 1.5×10^2 .

Figure 3 shows CT values in the pulmonary artery, left atrium, and aorta. The values of $\int C_{art}(t)dt$ are calculated for both calibration procedures, and they are considered reference values (the value for both calibration procedures is 1.00). If well calibrated, such as CT, these values were shown to be equal within 2% error.

Figure 4 shows the tracer concentrations in the same 3 regions as in Figure 3 taken by MRI. The value of $\int C_{la}(t)dt$ is 16% higher, and $\int C_{aor}(t)dt$ is 15% higher than the reference value when using the

Table 5 Blood Volume Contribution of Each Input and Comparison Between the 2 Calibration Procedures			
Calibration	$\int rBV_{art}$	$\int rBV_{aor}$	CP-PS Perfusion
Linear	318.0 mL	74.7 mL	23.5%
Eq. (5)	303.3 mL	62.4 mL	20.5%

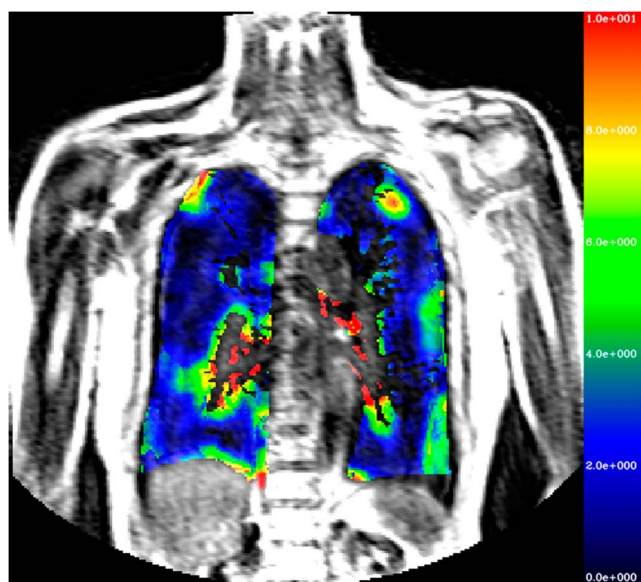


FIGURE 7: Slice 07 showing the result of the local analysis for rBV_{aor} (contribution from the aorta). An overestimate occurs near the spinal cord, probably because the aorta was included in the region of interest.

conventional linear approximation. With the proposed calibration, $\int C_{la}(t)dt$ is 2% and $\int C_{aor}(t)dt$ is 0% higher than the reference. The proposed model showed a smaller difference in the integral values of the pulmonary artery, left atrium, and aorta than the linear model.

Table 3 presents the results and averages for the 6 patients. In the linear approximation, the left atrium and aorta were 13% and 10% larger than the pulmonary artery, but these were suppressed to 5% and -1% by the proposed method.

Multiple Input BF Analysis Results

An example of a patient A, with the contribution of each input to the pulmonary perfusion, is shown in Figure 5. The contribution from each input can be analyzed separately because of the time difference. The peak is reached around 6.5 seconds, and the correspondence between $C_{art}(t) \otimes R_{art}(t)$ and the observed data is good considering the time interval without the influence of the second input, the aorta contribution. Near 13 seconds, the contribution from the pulmonary artery reaches approximately 0 mmol/mL, and the correspondence between $C_{aor}(t) \otimes R_{aor}(t)$ and the observed data has good correspondence. By summing the contributions from both inputs, a good correspondence with the observed data is obtained. There is only 1 possible outlier near the time instant of 19 seconds.

Figure 6 shows the results of the local analysis. In particular, (Figure 6F) and (Figure 6G) show that the blood contribution of the bronchial artery is greater and supports the cancer cells receiving arterial blood.

Table 4 presents the results for left and right cardiac output. The stroke volume for 1 cardiac output and the cardiac output volume per second are estimated according to the estimated heart rate. The difference between the cardiac output is 4.3 mL/s and represents CP-PS and 4.3 mL/s represents 6.2% of the output from the right ventricle, which is 69.2 mL/s. CP-PS has 6.2% of the whole BV. CP-PS is the l parameter used in expression Eq. (1).

Table 5 presents the results for $\int rBV_{art}$ and $\int rBV_{aor}$ considering both calibration procedures: the conventional linear approximation and the one proposed here. For both calibration methods, the CP-PS was greater than 20%.

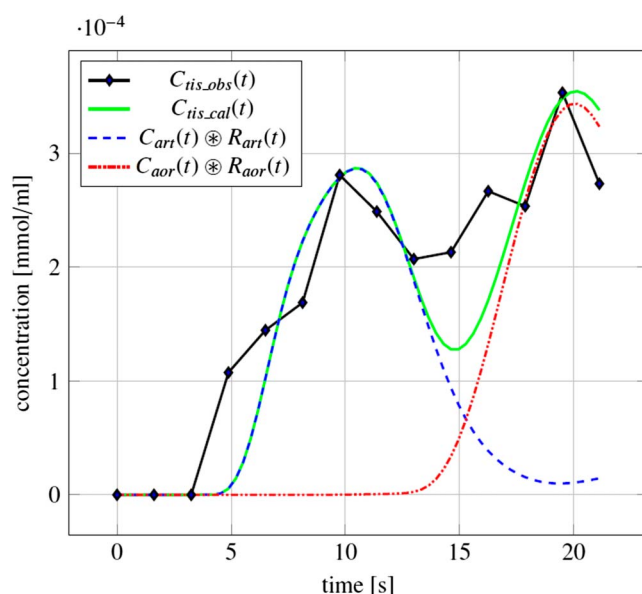


FIGURE 8: Result of the local analysis in the voxel inside the lung with overestimation of rBV_{aor} . The selected voxel can probably not be associated with the same point in space over time and belongs to the aorta in the final 5 seconds.

DISCUSSION

Calibration Model Consideration

As presented in Table 3, the proposed calibration still produces errors in $\int C_{la}(t)dt$ and $\int C_{aor}(t)dt$. This might originate from a different source of errors: imaging errors (such as patient movement during acquisition and segmentation problems), the inverse characteristic of contrast agents, and others.

The first is the imaging error. Considering Figure 3, even in CT, $\int rBV_{la}$ has a value 1% higher than the reference and $\int rBV_{aor}$ has a value 2% higher than the reference. The sampling rate was cited as the cause of this: 2.05 seconds/frame for CT and 1.62 seconds/frame for MRI. This low sampling rate may have caused errors in the integrated values.

The second is the inverse characteristic of contrast agents. When the concentration of the MRI contrast agent is too high, the contrast characteristic is reversed and the intensity of the MR signal reduces, as shown in Figure 2. In this study, the reverse characteristic was not considered. Because the contrast agent concentration reached near 0.03 mmol/mL in the pulmonary artery, the effect is not serious. However, a calibration procedure that includes this feature is desired and can be used in future experiments.

Difference Between Left and Right Cardiac Output

In this section, we discuss the error between the CP-PS obtained from the difference between the left and right cardiac

Table 6 Contribution of Blood Volume From Each Input Without Boundary Contraction (0 pixels) and With Boundary Contraction (3 pixels)

Contraction	$\int rBV_{art}$	$\int rBV_{aor}$	CP-PS Perfusion
0 pixels	303.3 mL	62.4 mL	20.5%
3 pixels	193.4 mL	26.1 mL	13.5%

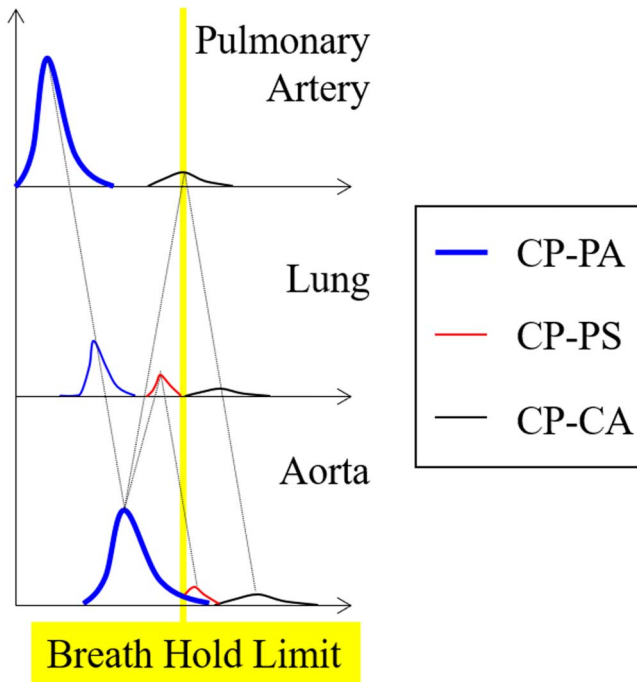


FIGURE 9: Three circulatory paths (CP-PA, CP-PS, and CP-CA) are represented at 3 different locations (pulmonary artery, lungs, and aorta). The breath hold limit is represented by a yellow vertical line.

output of patient A (6.2%) and the CP-PS obtained by the proposed multiple-input analysis (20.5%). The discrepancy between both CP-PS is 14.3%.

The first is the influence of thick blood vessels near the lung boundary. Figure 7 shows the results of a local analysis rBV_{aor} in a thick slice. It is possible to observe an overestimation of BV values in the region near the spinal cord. One possibility is the inclusion of the aorta in the region of interest (ROI). Figure 8 also shows this overestimation for a specific voxel. The concentration associated with the second input increases greatly, and one possibility is that the parenchymal tissue, such as the intercostal muscle, has reached the thickness of the slice of 12 mm.

In this additional experiment, a threshold value was set to exclude thick blood vessels from the ROI. The threshold cannot be too reduced because it is necessary to detect lung cancer, and consequently, some large vessels are included in the ROI. Trying to overcome the influence of some thick blood vessels near the lung boundary, a morphology contraction operation was performed and ROI was reduced by 3 pixels. Table 6 presents the results with a 3-pixel contraction; the ratio between $\int rBV_{art}$ and $\int rBV_{aor}$ improved by approximately 7%, from 20.5% to 13.5%. However, because the lung boundary BV was not considered for pulmonary artery input, the $\int rBV_{art}$ value decreased by 109.9 mL. Blood oxygenates at the lung boundary through the pulmonary alveolus, and a higher contrast concentration is expected. Considering this fact, a better proposal is required to define ROI, in which the contribution of each input of contrast concentration is considered. A higher concentration of the first input represents blood oxygenation near the lung boundary, and a higher concentration of the second input represents oxygenated blood going through thick vessels. Figure 8 combines the internal part of the lung with a high peak originating from the pulmonary artery and the external part of the lung with a high peak of oxygenated blood originating from the aorta. The cause of this

combination may be the proximity between the lung boundary and a thick vessel and/or the occurrence of internal involuntary movement.

The second is that we consider the influence of the CP-CA (coronary artery) as an overestimation of the perfusion of the bronchial artery. Figure 9 shows the influence of 3 circulatory paths (CP-PA, CP-PS, and CP-CA) at 3 different locations (pulmonary artery, lungs, and aorta). The contrast is injected and goes through the pulmonary artery and then through the lungs and aorta. This contribution comes from CP-PA and is represented by a blue curve. When it reaches the aorta, the BF splits into 3 different circulatory paths. Two of them are represented here: CP-PS and CP-CA. CP-PS enters the lungs and then returns to the aorta. It is represented by a red curve. CP-CA enters the heart and then enters the pulmonary artery, lungs, and aorta. It is represented by a black curve. In CP-CA, it takes approximately 8 ± 2 seconds to go from the coronary artery to the coronary vein.¹⁶ However, the subject can hold his/her breath for a limited time and starts breathing before coronary circulation is observed in the lung. Therefore, it is inferred that the acquisition of the contribution from CP-CA was interrupted, causing an overestimation of blood perfusion in the pulmonary artery. Considering Eq. (5), the perfusion from CP-CA was included in C_{in} , but it was not included in C_{tis} ; this situation caused a relative overestimation of the pulmonary artery.

Figure 4 shows a small increase in perfusion in the pulmonary artery near 19 seconds, approximately 8 seconds after the peak of aorta perfusion (the peak occurred around 11 seconds). This is approximately the time that the blood must travel from the coronary artery to the coronary vein.¹⁶ The same happens in Figure 3, where a second peak appears near 26 seconds that is 10 seconds after the peak of aorta perfusion (the peak occurred around 16 seconds). The time difference indicates that the additional perfusion appearing in Figures 3 and 4 can be derived from CP-CA.

An estimation of the contribution of the coronary artery can be performed by displacing the aorta graph by 10 seconds; this way, the peak of the aorta graph will be placed near 26 seconds. The translated graph is scaled to coincide with the peak near 26 seconds on the pulmonary artery curve. The resulting graph is shown in yellow in Figure 10. This is a virtual coronary contribution to the pulmonary artery. The $\int C_{cor}(t)dt$ in the pulmonary artery has 13%

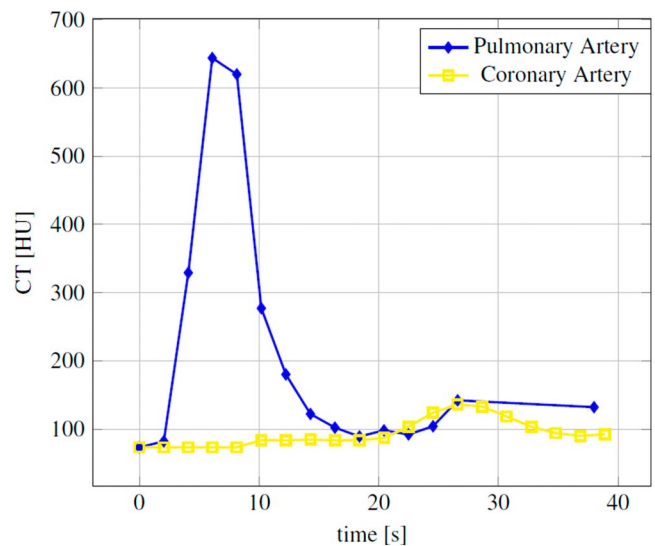


FIGURE 10: Tracer concentration is shown in the pulmonary artery with an evaluation of the contribution from the coronary artery (CP-CA circulatory path).

of BV in the pulmonary artery. The value of 13% is an overestimate that could include the perfusion of some organs near the lung, such as the liver. CP-CA is known to have approximately 5% of the right cardiac output.

The last is the reperfusion error. Eq. (1) considers an infinite number of iterations. However, only 2 iterations are considered in the experiments. It is necessary to evaluate the error present in the calibration performed considering only 2 iterations. The results presented in Table 4 show that $l = 6.2\%$. Considering just 2 iterations after truncating Eq. (1), we have

$$\frac{1 + 2l}{1 + l} = 1.058.$$

Changing $l = 6.2\%$ in Eq. (1), after infinite iterations, we get 1.062, the error is approximately 0.4% and can be ignored.

CONCLUSIONS AND FUTURE WORKS

A new calibration method is proposed based on the circulatory system, considering the minimum variation of the integral of the contrast concentration in time. Because no phantom is required in the proposed calibration method, it is cheaper. This is a great advantage.

The proposed single-input method is not influenced by reperfusion or noise generated by aliasing. The two-input method allowed the separation of functional and nutritional vasculature analysis. Six subjects considered having lung cancer, and a large perfusion with oxygenated blood from the aorta was observed. Comparison of rBV integrals for each input contribution with the Fast GE Cine method showed a discrepancy of approximately 14%. This discrepancy might happen because of the inability to perform perfect lung segmentation. Some thick blood vessels are near the lung boundary and influence local analysis.

Future research is intended to improve the determination of ROI, removing higher oxygenated blood peaks near the lung boundary. Current BF analysis is limited by the subject's ability to hold his breath. For example, Eq. (5) should use not only l SI(0) but also the average of multiple images before contrast injection. Future research also intends to improve the registration procedure to allow the same analysis to occur without this limitation.

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