

Evaluation of beam shape coefficients in T-matrix methods using a finite series technique: on blowing-ups using hypergeometric functions and generalized Bessel polynomials

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Abstract: In T-matrix methods (Generalized Lorenz-Mie theories or Extended Boundary Condition method), beam shape coefficients encoding the shape of the illuminating structured beam have to be evaluated. This may be carried out by using the finite series technique which, however, generates blowing ups when the partial wave order of the beam shape coefficients increases. Using hypergeometric functions and generalized Bessel polynomials, we demonstrate in the case of on-axis Gaussian beams that these blowing-ups are genuine phenomena, not due to a lack of numerical precision, and we establish criteria to evaluate the critical partial wave order which implies blowing-ups.

1. Introduction

T-matrix methods relate the scattered fields and the illuminating fields when a beam illuminates a scatterer. Such a method is constituted by the analytical generalized Lorenz-Mie theory (GLMT), more generally by generalized Lorenz-Mie theories (using the plural) [1–3], dealing with scattering particles which possess a sufficient degree of symmetry to allow for the use of the method of separation of variables [4–6]. Another example is the semi-analytical Extended Boundary Condition Method (EBCM), which is very often erroneously taken as synonymous of T-matrix, and which may deal with irregular particles [7, 8]. EBCM is mostly used in the case of plane wave illumination but illumination by structured beams may be considered as well, e.g. [9–13], see as well [3], Section 8.1, for a more extended discussion.

In such light scattering approaches, the illuminating structured beam is decomposed over a set of Vector Spherical Wave Functions (VSWFs) and expansion coefficients are best expressed in terms of beam shape coefficients (BSCs) which, in spherical coordinates, are denoted as $g_{n, TM}^m$ and $g_{n, TE}^m$ (TM: Transverse Magnetic; TE: Transverse Electric). In the case of on-axis Gaussian beams considered in the present paper, the double set $g_{n, TM}^m$ and $g_{n, TE}^m$ of BSCs reduces to a single uni-index set of special BSCs denoted g_n (n from 1 to ∞), which does not distinguish any more between TM and TE waves.

There are several methods used to the evaluation of beam shape coefficients, including quadratures [14, 15], localized approximation [16–19], finite series [20, 21], or the use of Angular Spectrum Decomposition [22–28].

Due mainly to the success of the localized approximations, the finite series method until recently disappeared from the stage during about three decades, excepted for a very small number of cases, two in an acoustical context [29, 30], and one in an electromagnetic context [31]. However, the recent discovery of limitations of localized approximations when the illuminating beam exhibits an axicon angle [32–36] and/or a topological charge [37–40], induced a revival of the finite series technique [39, 41–44].

46 It has then been observed that BSCs blow-up when the partial wave order of the BSCs increases,
 47 as summarized in [6], pp.168-171. In this reference, numerical observations for on-axis Gaussian
 48 beams have lead to the conclusion that blowing-ups are not the result of computational inaccuracy
 49 but no firm mathematical demonstration of this conclusion were established. Also, whether
 50 blowing-ups were consistent with physics remained an open problem. Blowing-ups have been
 51 observed as well in [39] in the case of Laguerre-Gauss beams freely propagating and in [44]
 52 for Laguerre-Gauss beams focused by a lens. In this last paper, blowing-ups were attributed
 53 to numerical inaccuracies, but it is suspected that, although numerical inaccuracies may be
 54 a source of blowing-ups, they might exist a genuine mathematical reason (connected with a
 55 physical explanation) for blowing-ups. The aim of the present paper is then to demonstrate
 56 within the framework of a firm mathematical demonstration, using hypergeometric functions and
 57 generalized Bessel polynomials, that blowing-ups indeed are a real phenomenon. Beside criteria
 58 to evaluate critical values of the partial wave order are proposed.

59 The paper is organized as follows. Section 2 describes the on-axis Gaussian beams to be
 60 examined either from a Davis scheme of approximations or as a special case of Laguerre-Gauss
 61 beams and shows how these two different approaches may be unified. Section 3 demonstrates
 62 that blowing-ups must indeed occur and establishes criteria for the critical values of the partial
 63 wave order. Such theoretical criteria can be directly compared with the “empirical” criterion
 64 recently proposed by Ambrosio and Gouesbet when dealing with computational calculations of
 65 the beam shape coefficients in acoustic scattering from ultrasonic Bessel beams, using a finite
 66 series method [45]. Section 4 exhibits numerical examples of blowing-ups and, using these
 67 numerical examples, criteria for critical values are tested. Section 5 is a conclusion.

68 **2. On-axis Gaussian beams.**

69 *2.1. From the Davis scheme of approximations.*

70 Gaussian beams may be described by using the Davis scheme of approximations [46,47] in which
 71 the fields take the form of series in terms of powers of a small parameter s , which may be named
 72 the beam confinement parameter, given by [6]:

$$s = \frac{w_0}{l} = \frac{1}{kw_0} \quad (1)$$

73 in which w_0 is the beam waist radius, l the diffraction length and k the wave-number. The
 74 successive approximations are called the first-, third-, fifth-order ... approximations and, although
 75 the scheme eventually diverges, in a way similar to the one observed in quantum electrodynamics
 76 [48], the first-order approximation is already a quite decent paraxial approximation to the
 77 description of Gaussian beams. Assuming a further simplification of the first-order scheme, we
 78 may obtain simple expressions for on-axis Gaussian beams finite series when the beam waist
 79 center of the beam coincides with the origin of coordinates used to describe the beam, according
 80 to Eqs.(39)-(40) in [20], and Eqs.(6.151)-(6.152) in [6]:

$$g_{2p+1} = \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(p+q+3/2)}{\Gamma(p+3/2)} (-4s^2)^q \quad (2)$$

$$g_{2p+2} = \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(p+q+5/2)}{\Gamma(p+5/2)} (-4s^2)^q \quad (3)$$

81 for n odd and even, respectively (p from 0 to ∞). Details will be provided in this paper for n odd
 82 only. The strong similarity between Eqs.2 and 3 should be enough to convince the reader that
 83 results obtained from n odd would become valid as well, *mutatis mutandis*, for n even as well.

84 **2.2. From Laguerre-Gauss beam description.**

85 In the case of paraxial Laguerre-Gauss beams freely propagating [39,41], BSCs obtained from
86 the finite series technique for n odd read as, e.g. Eqs.(68), (70) of [41]:

$$\begin{aligned} [g_{n,TM}^{\nu+1}]_{\mu} &= \frac{i^n \sqrt{\pi}}{2^{\nu+2}} \frac{(-1)^{(n+\nu+1)/2}}{\Gamma(\frac{n+\nu}{2} + 1)} \left(\frac{n-\nu-1}{2}\right)! \\ &\times \sum_{m=0}^{\leq n/2} 2^{\frac{1}{2}+n-2m} \frac{\Gamma(\frac{1}{2}+n-m)}{m!} [b_{n-2m}]_{\mu}, \\ \text{for } n &\geq \nu+1, (n-\nu) \text{ odd}, \nu \geq 0 \end{aligned} \quad (4)$$

$$\begin{aligned} [g_{n,TM}^{-1}]_{\mu} &= \frac{i^n \sqrt{\pi}}{4} \frac{(-1)^{(n+1)/2}}{\Gamma(\frac{n}{2} + 1)} \left(\frac{n-1}{2}\right)! \\ &\times \sum_{m=0}^{\leq n/2} 2^{\frac{1}{2}+n-2m} \frac{\Gamma(\frac{1}{2}+n-m)}{m!} [b_{n-2m}]_{\mu}, \\ \text{for } n &\geq 1, n \text{ odd} \end{aligned} \quad (5)$$

87 in which $[b_{n-2m}]_{\mu}$ are coefficients which, for the time being, do not need to be specified, and ν ,
88 μ are supercript and subscript to specify the Laguerre-Gauss polynomial L_{ν}^{μ} used to describe the
89 Laguerre-Gauss beams at hand. Gaussian beams may be deduced from Laguerre-Gauss beams
90 by specifying $\mu = \nu = 0$. The BSCs of Eqs.4 and 5 may then be unified in a single expression
91 reading as:

$$\begin{aligned} [g_{n,TM}^{\pm 1}]_0 &= \frac{i^n \sqrt{2\pi}}{4} \frac{(-1)^{(n+1)/2}}{\Gamma(\frac{n}{2} + 1)} \left(\frac{n-1}{2}\right)! \\ &\times \sum_{q=0}^{\leq n/2} 2^{n-2q} \frac{\Gamma(\frac{1}{2}+n-q)}{q!} [b_{n-2q}]_0 \end{aligned} \quad (6)$$

92 From Eq.(54) of [41], and using as well Eqs.(45) and (52), we obtain:

$$[b_{n-2q}]_0 = \frac{is}{\sqrt{2\pi}} \frac{(-s^2)^{(n-2q-1)/2}}{(\frac{n-2q-1}{2})!} \quad (7)$$

93 Inserting Eq.7 into Eq.6 and restricting ourselves to the case $n = 2p + 1$ odd, as in subsection
94 2.1, we obtain:

$$[g_{2p+1,TM}^{\pm 1}]_0 = P \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(2p-q+3/2)}{\Gamma(p+3/2)} \left(\frac{-1}{4s^2}\right)^q \quad (8)$$

95 in which P is a pre-factor reading as:

$$P = (-1)^p s^{2p+1} 2^{2p-1} \quad (9)$$

96 We then omit the pre-factor (which is equivalent to a choice of normalization), and rewrite
97 Eq.8 as:

$$(g_{2p+1})_{LG} = S_p = \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(2p-q+3/2)}{\Gamma(p+3/2)} \left(\frac{-1}{4s^2}\right)^q \quad (10)$$

98 2.3. Unified scheme

99 Since Eqs.2 and 10 both describe a paraxial Gaussian beam, we should expect a strong relationship
100 between both of them. Indeed, using Eq.10, we establish:

$$(-4s^2)^p S_p = \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(2p-q+3/2)}{\Gamma(p+3/2)} (-4s^2)^{p-q} \quad (11)$$

101 Then, setting $(p-q) = u$ in Eq.11, and eventually changing u to q , we readily establish:

$$(-4s^2)^p S_p = \sum_{q=0}^p \binom{p}{q} \frac{\Gamma(p+q+3/2)}{\Gamma(p+3/2)} (-4s^2)^q \quad (12)$$

102 which relates $S_p = (g_{2p+1})_{LG}$ and g_{2p+1} of Eq.2.

103 3. Blowing-ups of beam shape coefficients

104 3.1. Coefficients must blow-up

105 In this section, we shall demonstrate that BSCs must blow-up. We shall use hypergeometric
106 functions whose relevant properties are summarized in the Appendix for the convenience of the
107 reader. Let us then consider g_{2p+1} of Eq.2. It may be rewritten as a hypergeometric series (see
108 Appendix for notations and properties):

$$g_{2p+1} = \sum_{q=0}^p c_q (4s^2)^q \quad (13)$$

109 in which c_q is a hypergeometric term:

$$c_q = (-1)^q \binom{p}{q} \frac{\Gamma(p+q+3/2)}{\Gamma(p+3/2)} \quad (14)$$

110 from which we derive, after rearranging, using $\Gamma(p+1) = p\Gamma(p)$:

$$\frac{c_{q+1}}{c_q} = \frac{q-p}{q+1} (p+q+3/2) \quad (15)$$

111 which using Eq.50, leads to:

$$\begin{aligned} g_{2p+1} &= \sum_{q=0}^p c_q (4s^2)^q \\ &= {}_2F_0 \left(\begin{matrix} -p, p+3/2 \\ - \end{matrix} ; 4s^2 \right) = {}_2F_0(-p, p+3/2; ; 4s^2) \end{aligned} \quad (16)$$

112 Another way to express g_{2p+1} is to use the identity [49]:

$${}_{N+1}F_M \left(\begin{matrix} -m, \mathbf{a} \\ \mathbf{b} \end{matrix} ; z \right) = \frac{(\mathbf{a})_m}{(\mathbf{b})_m} (-z)^m \cdot {}_{M+1}F_N \left(\begin{matrix} -m, 1-m-\mathbf{b} \\ 1-m-\mathbf{a} \end{matrix} ; \frac{(-1)^{N+M}}{z} \right) \quad (17)$$

113 In particular, we may check with a bit of effort that:

$$g_{2p+1} = {}_2F_0\left(\begin{matrix} -p, p+3/2 \\ - \end{matrix}; 4s^2\right) \quad (18)$$

$$= (p+3/2)_p (-4s^2)^p {}_1F_1\left(\begin{matrix} -p \\ -2p-1/2 \end{matrix}; \frac{-1}{4s^2}\right)$$

114 Instead of using hypergeometric functions, we may use generalized Bessel polynomials defined
115 as [50, 51]:

$$y_p(x; a, b) = \sum_{q=0}^p \binom{p}{q} (p+a-1)_q \left(\frac{x}{b}\right)^q \quad (19)$$

116 From now on, it will be sufficient to use $b = 2$ so that we may use the notation:

$$y_p(x; a, b) = y_p(x; a, 2) = y_p(x; a) \quad (20)$$

117 We then establish:

$$g_{2p+1} = y_p(-4s^2; \frac{5}{2}, 1) = y_p(-8s^2; \frac{5}{2}, 2) = y_p(-8s^2; \frac{5}{2}) \quad (21)$$

118 However, there exists an asymptotic expression for the generalized Bessel polynomials which,
119 for large p and $x \neq 0$, reads as ([51], Chapter 13, Theorem 3):

$$y_p(x; a) = \left(\frac{2px}{e}\right)^p 2^{a-3/2} e^{1/x} \left[1 - \frac{1}{24p} - \frac{1}{4px^2} - (a-2) \frac{a-1+2/x}{4p} + O\left(\frac{1}{p^2}\right)\right] \quad (22)$$

120 When p is sufficiently large the behavior of $y_p(x; a)$ is then governed by $(px)^p$ which,
121 therefore, must blow up.

122 3.2. *Blowing-up criteria*

123 Criteria for blowing-ups are defined by critical values of p denoted p_c and associated critical
124 values of partial wave orders n denoted n_c which are equal to $2p_c + 1$. We shall propose and
125 test three theoretical criteria. The first one relies on Eq.22. When p is sufficiently large, the
126 blowing-up criterion is governed by the leading term $(2px/e)^p$ and the blowing-up criterion is
127 then obtained when this term begins to increase indefinitely when p increases, so that we have a
128 first blowing-up criterion given by:

$$\frac{2p_c |x|}{e} \sim 1 \quad (23)$$

129 From Eq.21, we have $x = -8s^2$, so that:

$$p_c \sim \text{int}\left(\frac{e}{16s^2}\right) \sim \text{int}(0.170/s^2) \quad (24)$$

130 leading to:

$$n_c \sim \text{int}(0.340/s^2) + 1 \quad (25)$$

131 in which $\text{int}(x)$ is the integer closest to x .

132 Instead of using generalized Bessel polynomials, we may evaluate criteria using hypergeometric
 133 functions. Eq.12 shows that S_p and $(2p+1)$ generate identical critical values. As a variant to the
 134 use of g_{2p+1} to establish Eq.25, we shall now deal with Eq.10 to evaluate new critical values. We
 135 rewrite Eq.10 as:

$$S_p = \sum_{q=0}^p T_q \quad (26)$$

136 in which:

$$T_q = \binom{p}{q} \frac{\Gamma(2p-q+3/2)}{\Gamma(p+3/2)} \left(\frac{-1}{4s^2}\right)^q \quad (27)$$

137 We observe that S_p of Eq.26 is an alternating series. Assuming that p is odd (the case p even
 138 would be treated similarly), we may rewrite S_p as:

$$\begin{aligned} S_p &= \sum_{q=0}^p T_q = (T_0 + T_1) + (T_2 + T_3) + \dots + (T_{p-1} + T_p) \\ &= \sum_{q=0, \text{even}}^{p-1} (T_q + T_{q+1}) \end{aligned} \quad (28)$$

139 We then define, still with q even:

$$R_q = \frac{T_{q+2} + T_{q+3}}{T_q + T_{q+1}} \quad (29)$$

140 and set the criterion to a critical value of $p = p_c$ such as:

$$R_q(p_c) \sim 1 \quad (30)$$

141 From Eq.27, we establish that:

$$\begin{aligned} T_{q+2} + T_{q+3} &= \frac{\Gamma(2p-q-3/2)}{\Gamma(p+3/2)} \frac{p!}{(q+2)!(p-q-3)!} \left(\frac{-1}{4s^2}\right)^{q+2} \\ &\times \left(\frac{2p-q-3/2}{p-q-2} + \frac{1}{q+3} \frac{-1}{4s^2}\right) \end{aligned} \quad (31)$$

142 from which we immediately derive:

$$\begin{aligned} T_q + T_{q+1} &= \frac{\Gamma(2p-q+1/2)}{\Gamma(p+3/2)} \frac{p!}{(q)!(p-q-1)!} \left(\frac{-1}{4s^2}\right)^q \\ &\times \left(\frac{2p-q+1/2}{p-q} + \frac{1}{q+1} \frac{-1}{4s^2}\right) \end{aligned} \quad (32)$$

143 so that, after rearranging, we obtain:

$$\begin{aligned} R_q &= \frac{p-q-1}{(q+1)(q+2)} \left(\frac{-1}{4s^2}\right)^2 \\ &\times \frac{(2p-q-3/2) + (p-q-2) \frac{1}{q+3} \frac{-1}{4s^2}}{\frac{2p-q+1/2}{p-q} + \frac{1}{q+1} \frac{-1}{4s^2}} \end{aligned} \quad (33)$$

144 which can be rearranged to:

$$R_q = \frac{(p-q-1)(p-q)}{(q+2)(q+3)} \left(\frac{1}{4s^2} \right)^2 \times \frac{(2p-q-3/2)(q+3)4s^2 - (p-q-2)}{(2p-q+1/2)(q+1)4s^2 - (p-q)} \quad (34)$$

145 It is numerically observed that the successive terms of the series begin to decrease when p
 146 decreases (see next Section). Then, a blowing-up criterion is obtained when this trend begins
 147 to be false so that the most dangerous value of q is the one at the top level of the summation.
 148 Comparing Eq.28 in which the summation ends with T_p and Eq.29 in which the highest-order
 149 term has an order equal to $(q+3)$, we see that the most dangerous term in R_q is for $p = q+3$, i.e.
 150 $q = p-3$. Therefore to apply the criterion of Eq.30, we have to evaluate R_q for $q = p-3$ (note
 151 that q is even, which agrees with the fact that p is odd). We readily obtain:

$$R_{p-3} = \frac{6}{p(p-1)} \left(\frac{1}{4s^2} \right)^2 R_F \quad (35)$$

152 in which:

$$R_F = \frac{4p(p+3/2)s^2 - 1}{4(p-2)(p+7/2)s^2 - 3} \quad (36)$$

153 We shall now distinguish two regimes. In Regime 1, we assume that the critical p is so large
 154 (this will depend on the value of s) that we neglect the integers (-1) and (-3) in the numerators
 155 and denominators of Eq.36. Then, we have:

$$R_F \sim 1 \quad (37)$$

156 so that the critical p is given by:

$$\frac{6}{p_c^2} \left(\frac{1}{4s^2} \right)^2 \sim 1 \quad (38)$$

157 leading to:

$$p_c \sim \text{int}\left(\frac{\sqrt{6}}{4} \frac{1}{s^2}\right) \quad (39)$$

158 and to:

$$n_c \sim \text{int}\left(\frac{\sqrt{6}}{2} \frac{1}{s^2}\right) + 1 \sim \text{int}(1.224/s^2) + 1 \quad (40)$$

159 which departs significantly from the criterion of Eq.25.

160 In Regime 2, we assume the values of p and s work together so that we may neglect, in the
 161 numerators and denominators of Eq.12, the algebraic terms with respect to the integers. Then:

$$R_F \sim 1/3 \quad (41)$$

162 so that the critical p is given by:

$$p_c \sim \text{int}\left(\frac{\sqrt{2}}{4} \frac{1}{s^2}\right) \quad (42)$$

163 so that the critical value of n is:

$$n_c \sim \text{int}\left(\frac{\sqrt{2}}{2} \frac{1}{s^2}\right) + 1 \sim \text{int}(0.353/s^2) + 1 \quad (43)$$

164 which is close to the result given by Eq.25.

165 Furthermore, these last evaluations provide as well a complementary demonstration, using
166 hypergeometric functions, that BSCs must blow up.

167 Another blow-up criterion has also been recently proposed in the framework of acoustic
168 scattering when dealing with the Finite Series method for ultrasonic Bessel beams. Based on
169 computational calculations, Ambrosio and Gouesbet suggested an empirical critical value for n
170 of the form [45]:

$$n_c \sim \text{int}\left(\frac{3}{8s^2}\right) \sim \text{int}(0.375/s^2) \quad (44)$$

171 which shall be used in the next section in comparison with the three theoretical criteria discussed
172 above.

173 4. Numerical results

174 In order to assess the accurateness of the critical criteria derived in the previous section and
175 given by Eqs. (24), (39) and (42), an algorithm has been written using the commercial software
176 *Mathematica* (Wolfram, 12.1 Student Edition) and is available upon request. All simulations
177 were run on a personal laptop with the following configuration: Intel(R) Core(TM) i7-3630QM
178 CPU @ 2.40GHz, 16.0 GB.

179 Equation (2) for g_{2p+1} has been implemented and investigated as a function of p for different
180 values of s . The three criteria in Eqs. (24), (39) and (42) are called “C1”, “C2” and “C3”,
181 respectively, while the empirical criterion $n_c \sim \text{int}(3/8s^2)$ ($n_c = 2p_c + 1$) [45], is here denoted
182 as “Emp”.

183 Figure 1 shows the natural logarithm of g_{2p+1} as a function of p for $s = 1/2\pi, 1/3\pi, 1/6\pi,$
184 $1/10\pi, 1/15\pi$, respectively. Inset figures have been included in Figs. ??(a)-(c) for better
185 visualization of the curves at regions close to the actual critical points.

186 For $s = 1/2\pi$, it is seen that the critical point above which g_{2p+1} starts to increase occurs at
187 $p = p_c = 7$. In addition, for this particular value of s , Eqs. (24), (39) and (42) gives $p_{c,C1} = 7$,
188 $p_{c,C2} = 24$ and $p_{c,C3} = 14$, while $p_{c,Emp} = 7$. Therefore, C2 and C3 predict critical points two
189 and more than three times the actual one. On the other hand, C1 and Emp exactly agrees with the
190 turning point seen in Fig. 1(a).

191 As the value of s increases, the critical p values predicted by criteria C1, C2 and C3 deviate
192 more and more from those actually observed through the figures. For example, $p_{c,C1} = p_{c,Emp} =$
193 $p_c = 7$ for $s = 1/2\pi$, but it is seen from Fig. 1(e) for $s = 1/15\pi$ that $p_c = 418$, but $p_{c,C1} = 377$,
194 $p_{c,C2} = 1360$ and $p_{c,C3} = 785$, while $p_{c,Emp} = 416$.

195 The discrepancy between Emp and C_i ($i = 1, 2, 3$) is expected, since the blowing-up criteria
196 established in Sec. 3.2 relies upon approximations and observations related to asymptotic
197 expressions, while the empirical criterion was previously postulated in Ref. [45] based upon
198 computational simulations of similar finite series and hypergeometric functions associated with
199 the beam shape coefficients of acoustic beams. Figure 2 shows the behavior of Eqs. (24), (39)
200 and (42) as a function of s , for $1/65 \leq s \leq 16/100$. The empirical criterion $n_c \sim \text{int}(3/8s^2)$ is
201 actually shown in terms of p_c . Notice that, as s increases, all criteria tend to converge to small
202 values of p_c , since they all carry a s^{-2} -dependence. The largest bound of $s = 0.16$ implies on a
203 Gaussian beam whose beam waist radius w_0 is approximate equal to the wavelength [52].

204 It becomes clear from the above results that C2 is the worst to be used as a blow-up criterion,
205 followed by C3 and C1. On the other hand, Emp is accurate for essentially the entire range of s .

206 Regardless of the criterion, however, it remains the fact that, counter-intuitive as it may seem at
 207 first, the beam shape coefficients derived from the finite series must eventually blow-up.

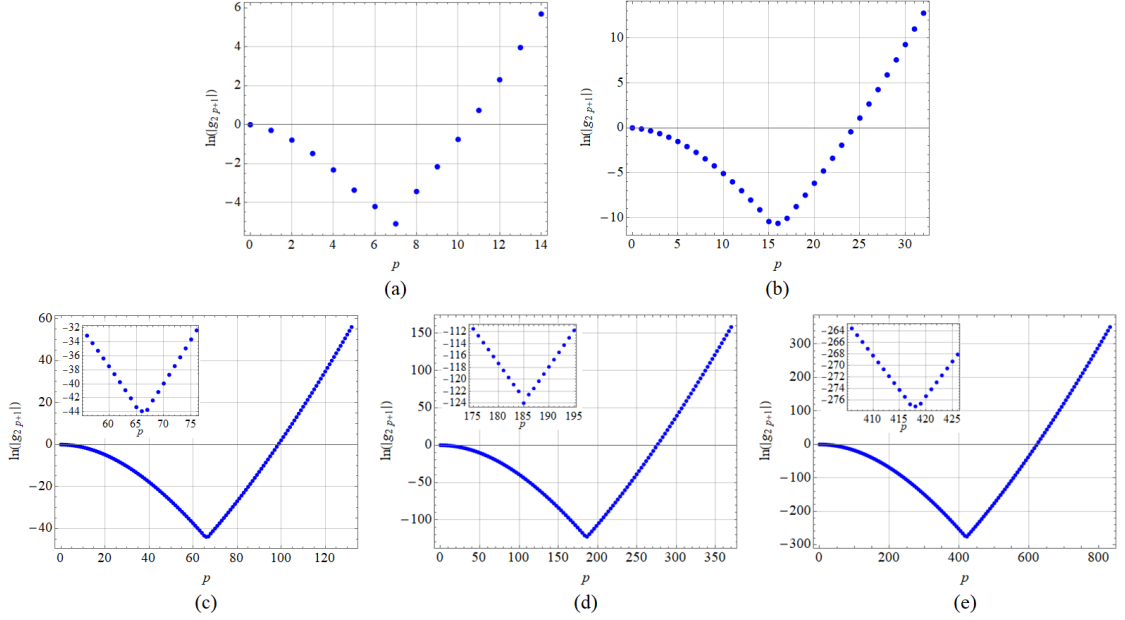


Fig. 1. Natural logarithmic of g_{2p+1} as a function of p for (a) $s = 1/2\pi$, (b) $s = 1/3\pi$, (c) $s = 1/6\pi$, (d) $s = 1/10\pi$ and (e) $1/15\pi$. Observed value of p_c and critical values associated with C1, C2, C3 and Emp are, respectively: (a) $p_c = 7$, $p_{c,C1} = 7$, $p_{c,C2} = 24$, $p_{c,C3} = 14$ and $p_{c,Emp} = 7$. (b) $p_c = 16$, $p_{c,C1} = 15$, $p_{c,C2} = 54$, $p_{c,C3} = 31$ and $p_{c,Emp} = 16$. (c) $p_c = 66$, $p_{c,C1} = 60$, $p_{c,C2} = 618$, $p_{c,C3} = 126$ and $p_{c,Emp} = 66$. (d) $p_c = 185$, $p_{c,C1} = 168$, $p_{c,C2} = 604$, $p_{c,C3} = 349$ and $p_{c,Emp} = 185$. (e) $p_c = 148$, $p_{c,C1} = 377$, $p_{c,C2} = 1360$, $p_{c,C3} = 785$ and $p_{c,Emp} = 416$.

208 5. Conclusion

209 In this paper we have therefore demonstrated, relying on the case of on-axis Gaussian beams,
 210 that blowing-ups observed when using the finite series technique to the evaluation of BSCs are
 211 not artefacts, but genuine mathematical consequences of the beam description. Using different
 212 methods, it may furthermore be demonstrated that these blowing-ups are not physical artefacts as
 213 well. They actually are physical ingredients required to describe evanescent waves [53].

214 Appendix.

215 The generalized hypergeometric function ${}_N F_M$ represents a series according to:

$${}_N F_M \left(\begin{matrix} a_1, \dots, a_N \\ b_1, \dots, b_M \end{matrix} ; z \right) = \sum_{q=0}^{\infty} \frac{(a_1)_q \dots (a_N)_q}{(b_1)_q \dots (b_M)_q} \frac{z^q}{q!} \quad (45)$$

216 in which $(x)_n$ is the Pochhammer symbol reading as:

$$(x)_0 = 1 \quad (46)$$

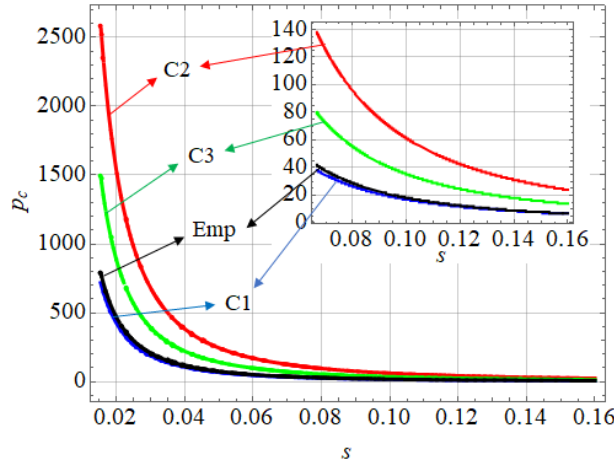


Fig. 2. p_c as a function of s for all four criteria (C1, C2, C3 and Emp). As s increases, the curves tend to converge to small values of p_c due to their s^{-2} -dependence.

$$(x)_n = \frac{\Gamma(x+n)}{\Gamma(x)} = x(x+1)\dots(x+n-1), n \neq 0 \quad (47)$$

Eq.45 may be written more concisely as:

$${}_N F_M \left(\begin{matrix} \mathbf{a} \\ \mathbf{b} \end{matrix} ; z \right) = {}_N F_M (\mathbf{a}; \mathbf{b}; z) = \sum_{q=0}^{\infty} \frac{(\mathbf{a})_q}{(\mathbf{b})_q} \frac{z^q}{q!} \quad (48)$$

Next, a series $\sum_{k=0}^{\infty} c_k$ is called a hypergeometric series, and c_k a hypergeometric term, if $c_0 = 1$ and if the ratio of two successive terms may be written as [54]:

$$\frac{c_{k+1}}{c_k} = \frac{P(k)}{Q(k)} = \frac{1}{k+1} \frac{(a_1+k)\dots(a_N+k)}{(b_1+k)\dots(b_M+k)} \quad (49)$$

We may then easily demonstrate that:

$$\sum_{k=0}^{\infty} c_k z^k = {}_N F_M \left(\begin{matrix} a_1, \dots, a_N \\ b_1, \dots, b_M \end{matrix} ; z \right) \quad (50)$$

Incidentally, one of the parameter row may be empty (if $N = 0$ or $M = 0$), then the row is noted by using a strike. As an example, the reader may check that the geometric series is equivalent to ${}_1 F_0$ according to:

$$\sum_{k=0}^{\infty} x^k = \frac{1}{1-x} = {}_1 F_0 \left(\begin{matrix} 1 \\ - \end{matrix} ; x \right) = {}_1 F_0(1;; x) \quad (51)$$

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