



## Biological activity of mullite macrospheres for bone tissue regeneration

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### ABSTRACT

The development of ceramic bone graft substitutes that combine mechanical strength, biocompatibility, and interconnected porosity remains a challenge, particularly for injectable applications. Mullite ( $\text{Al}_6\text{Si}_2\text{O}_{13}$ ) is a ceramic of particular interest due to its biocompatibility, chemical stability, and moderate mechanical properties; however, its use as a loose-fill implant has not yet been well explored. In this study,  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  macrospheres were fabricated via ionotropic gelcasting, using sodium alginate as the binder and colloidal silica as the silica source. Three compositions were investigated:  $\text{Al}_2\text{O}_3$ -rich, stoichiometric mullite, and  $\text{SiO}_2$ -rich. Thermal treatments at 1500 °C yielded mullite, cristobalite, and residual alumina in different ratios. All samples exhibited high sphericity and inter-sphere macroporosity, favorable for loose-fill bone graft applications. The stoichiometric mullite macrospheres demonstrated the most balanced combination of specific surface area, microhardness, abrasion resistance, and compressive strength. In vitro assays confirmed the absence of cytotoxic and hemolytic effects and demonstrated support for osteoblast adhesion, proliferation, and alkaline phosphatase activity. These findings indicate that  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  macrospheres, particularly stoichiometric mullite, are promising candidates for granular bone graft substitutes, offering a combination of structural integrity and biological performance suitable for bone tissue regeneration.

### 1. Introduction

A wide range of bioceramic materials is currently being developed for use in tissue regeneration and drug delivery, with characteristics tailored to their specific applications, particularly in the form of loose-fill implants [1]. Calcium phosphates ( $\text{Ca}_3(\text{PO}_4)_2$ ) are among the most extensively studied bioactive ceramics [1–5], while alumina ( $\text{Al}_2\text{O}_3$ ) and zirconia ( $\text{ZrO}_2$ ) are widely studied as bioinert materials [5–11]. The functionality and the inclusion of other materials or trace elements are essential points to enhance these materials' properties, as well as the development of new bioceramics or the optimization of synthesis processes. Biomaterials, such as calcium silicate ( $\text{CaSiO}_3$  or  $\beta$ -Wollastonite), which have bioactivity and degradability properties, are suitable for bone tissue regeneration [12,13]. Zhang et al. (2013) reported that the functionalization of the  $\text{CaSiO}_3$  with iron (Fe) resulted in a

multifunctional mesoporosity magnetic biomaterial suitable for bone regeneration, local drug delivery, and magnetic hyperthermia [13]. Ismail et al. (2021) studied how mullite ( $3\text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$ ), maghemite ( $\gamma\text{-Fe}_2\text{O}_3$ ), and silver (Ag) nanoparticles would improve the tensile strength, magnetism, bioactivity, and antimicrobial activity of  $\beta$ -Wollastonite. They reported that each dopant material improved one property, particularly at 20 wt% Mullite, which boosted compressive strength by up to 200 % making it suitable for cancellous bone applications [14].

Macrospheres are low-aspect-ratio, spherically-shaped materials with diameters ranging from 1 to 10 mm. Due to their loose-fill shape, they can access complex geometric areas, working as scaffolds with the spheres serving as the solid part and the vacancies between them as the porous phase. Several routes can produce spheres, including chemical reactions [15], sol-gel [16,17], spray-drying [18,19], foaming [20], and

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**Table 1**

Physicochemical characteristics of the raw materials used for the fabrication of  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  macrospheres, including chemical purity, particle size distribution, density, and specific surface area.

Characteristics	Calcined Alumina (CA) <sup>a</sup>	Colloidal Silica (CS) <sup>b</sup>
Composition (wt.%)	$\alpha$ - $\text{Al}_2\text{O}_3$ : 99.80; $\text{Na}_2\text{O}$ : 0.07; $\text{Fe}_2\text{O}_3$ : 0.02; $\text{MgO}$ : 0.05; $\text{SiO}_2$ : 0.03; $\text{CaO}$ : 0.02.	$\text{SiO}_2$ : 99.90; $\text{Na}_2\text{O}$ : 0.01.
Main crystalline phase (PDF file)	$\alpha$ - $\text{Al}_2\text{O}_3$ (46–1212)	$\text{SiO}_2$ (non-crystalline)
Particle Size ( $D_{10}$ , $D_{50}$ , $D_{90}$ )	0.27, 1.13, 14.02 [ $\mu\text{m}$ ]	11.31, 54.10, 87.08 [nm]
Solid Density [ $\rho$ , $\text{g}\cdot\text{cm}^{-3}$ ]	4.05	2.20
Specific surface area [ $\text{m}^2\cdot\text{g}^{-1}$ ]	8.20	80.00
Solid content [wt%]	–	50
Viscosity [cP]	–	8.00

(<sup>a</sup>) After thermal treatment at 1000 °C.

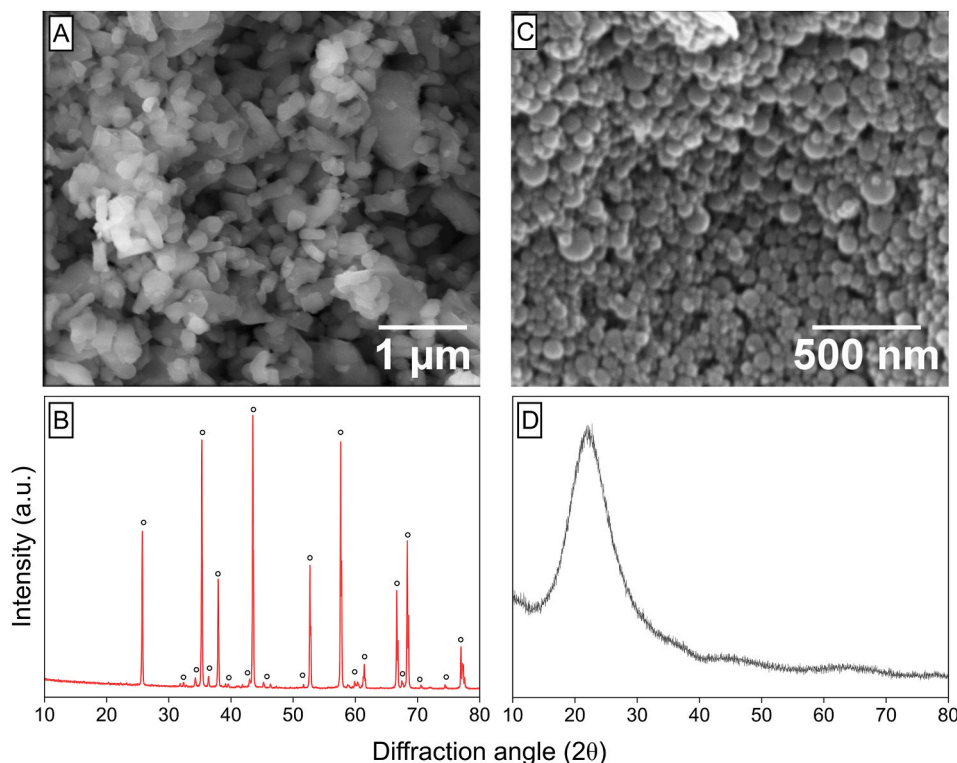
(<sup>b</sup>) After drying at 120 °C.

ionotropic gelation [21–23]. Ionotropic gelation stands out for its versatility and low cost, enabling the production of dense or porous structures from powders with varying particle sizes, resulting in pure or composite final products with good homogeneity and minimal defects. The spheroidization technique has been widely standardized to produce improved organic and inorganic sphere materials [23–25]. This technique consists of the consolidation and immobilization of particles through the formation of a polymeric network, produced by *in-situ* polymerization of organic monomers previously dissolved in stable suspensions in the presence of cross-linking agents [22,26].

Alumina ( $\text{Al}_2\text{O}_3$ ) is a well-known bioceramic due to its good stability in physiological environments, biocompatibility, and high resistance to compression and wear [6,8,27–29]. However, due to its low bioactivity, numerous studies attempted to combine  $\text{Al}_2\text{O}_3$  with bioactive materials,

such as hydroxyapatite [30–33], bioglass [34,35], keratin [36,37], silk fibroin [38], and chitosan [7,11]. Similarly, studies involving  $\text{SiO}_2$  composites are common in nanomedicine, particularly when combined with other biomaterials to improve bioactivity [4,39,40] or develop efficient drug delivery systems [15,19]. Additionally, mullite, a stable phase within the  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  system, is of particular interest due to its biocompatibility, chemical stability, and moderate mechanical properties. The biocompatibility of its constituent phases supports its potential as a biomaterial [41,42]. Over the past decades, mullite has been studied as a mechanical reinforcement [2,43] and, more recently, as an antimicrobial agent [44]. Although it has not yet been explored as a bone graft substitute, its cytocompatibility suggests promising potential for this application [42,45].

To meet the demands of bone graft substitutes, such as porosity for cell growth, vascularization, along with mechanical integrity and bioactivity, tailored microstructures and compositions are essential. The production of spherical ceramic granules with interconnected macroporosity can enhance implant packing, nutrient diffusion, and cell migration, thereby enhancing their suitability for bone defect repair. Nevertheless, achieving controlled porosity and phase composition while maintaining adequate mechanical and biological properties remains a significant challenge. This study aimed to produce  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  macrospheres using calcined alumina and colloidal silica. The macrospheres were produced by ionotropic gelcasting through an aqueous co-dispersion of calcined alumina and colloidal silica, employing sodium alginate as a binder. After drying and thermal treatments, macrospheres were characterized regarding their meso- and macroporosity distribution. Thermogravimetric and dilatometric analysis were conducted, along with microstructural, morphological, and mechanical strength characterizations. *In vitro* cytotoxicity, hemocompatibility, metabolic activity, cell adhesion, and alkaline phosphatase activity assays were performed to evaluate the biological response. The results provide insights into the design of ceramic spheres for potential use as injectable or loose-fill bone graft materials.

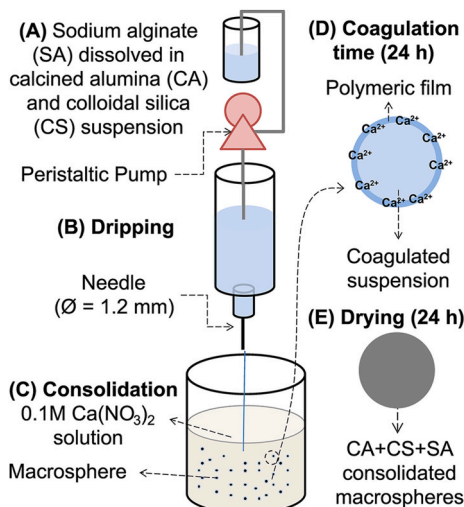


**Fig. 1.** SEM micrographs and XRD patterns of the raw materials used for macrosphere fabrication. (A, B) Calcined alumina (A1000SG: Corundum, JPCDS 1–1243). (C, D) Colloidal silica (Levasil CS 5028).

**Table 2**

Chemical composition design of the  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ceramics investigated, expressed in mol% and wt% to illustrate variations from stoichiometric mullite toward alumina- or silica-excess formulations.

Samples identification	Composition tested	$\text{Al}_2\text{O}_3$ [mol/wt %]	$\text{SiO}_2$ [mol/wt %]
3A1S (excess of alumina)	75 % mol $\text{Al}_2\text{O}_3$ 25 % mol $\text{SiO}_2$	3/83.58	1/16.42
3A2S (stoichiometric mullite)	60 % mol $\text{Al}_2\text{O}_3$ 40 % mol $\text{SiO}_2$	3/71.79	2/28.21
3A3S (excess of silica)	50 % mol $\text{Al}_2\text{O}_3$ 50 % mol $\text{SiO}_2$	3/62.92	3/37.08



**Fig. 2.** Ionotropic gelation process for the production of alumina-silica macrospheres. (A) is the preparation of ceramic/polymer suspension; (B) dripping process into a 1.2 mm needle; (C) consolidation in a 0.1 M  $\text{Ca}(\text{NO}_3)_2$  solution; (D) spheres remain 24 h in the gelling solution for formation of a polymeric film; (E) after washing, spheres are dried (60 °C, 24 h), obtaining the consolidated macrospheres.

## 2. Materials and methods

### 2.1. Preparation of suspensions

$\text{Al}_2\text{O}_3/\text{SiO}_2$  suspensions (Table 1) were prepared using distilled water, calcined alumina (CA,  $\alpha\text{-Al}_2\text{O}_3$ , A1000SG, Almatiss, USA), colloidal silica dispersions (CS, synthetic amorphous  $\text{SiO}_2$ , Levasil CS5028, Nouryon South America, Brazil), and sodium alginate (SA,  $\text{C}_6\text{H}_7\text{O}_6$ , Synth, Brazil) as a binder. A dispersant (poly(carboxylate ether), FS 20 Castment, BASF, Germany) and an anti-foam agent (Tensiol, Lamberti, Brazil) were added to improve particle individualization and prevent trapped air bubbles, respectively. A bath of calcium nitrate ( $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$ , Exodo Científica, 0.1 M) behaved as a coagulating agent.

All raw materials were previously characterized regarding composition (X-ray dispersive spectroscopy, Shimadzu, EDX 720), morphology (SEM, FEG-SEM Inspect-F50, FEI Company, the samples were fixed in carbon tape and sputter-coated with platinum (Q150R sputter, Quorum Technologies) for 1 min, Fig. 1A and B), crystalline phases (X-ray diffraction, Rotaflex RV 200B, Rigaku-Denki Corp., with  $\text{Cu K}\alpha$  radiation ( $\lambda = 0.14506$  nm), diffraction angle ( $2\theta$ ) scanned between  $10^\circ$  and  $100^\circ$ , rate of  $2^\circ \cdot \text{min}^{-1}$ ) (Fig. 1C and D), particle size distribution ( $D_{10}/D_{50}/D_{90}$ , DT-1202, Dispersion Technology Inc.), solid density (99.999 % purity helium pycnometry - Ultrapyc 1200e, Quantachrome Instruments), and specific surface area (SSA, BET method, Nova 1200e, Quantachrome Instruments, ASTM C 1069-09 standard “Standard Test

Method for Specific Surface Area of Alumina or Quartz by Nitrogen Adsorption” [46]).

The compositions tested (Table 2) were defined from different  $\text{Al}_2\text{O}_3\text{-SiO}_2$  ratios based on their phase diagram [47]: a stoichiometric mullite composition ( $3\text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$  or  $\text{Al}_6\text{Si}_2\text{O}_{13}$ ), one condition with excess of  $\text{Al}_2\text{O}_3$  ( $3\text{Al}_2\text{O}_3 \cdot 1\text{SiO}_2$ ), and another with excess of  $\text{SiO}_2$  ( $3\text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ ).

### 2.2. Synthesis of mullite macrospheres

The macrospheres were produced by dripping. Initially, sodium alginate (SA, 3 wt% of the total solids in suspension) was dissolved in distilled water (10 times the mass of SA). A 20 vol% of solids alumina suspension was prepared by adding calcined alumina (CA) powder and dispersant (0.1 wt%) in water. The mixture was ground in a ball mill (1:10 mass of solids/ $\text{ZrO}_2$  spheres, 6 mm, 80 rpm; SL34/4, SOLAB, Brazil) for 2 h to break agglomerates. The alumina suspension was added to the polymeric solution and homogenized for 10 min with a paddle mixer (RW 20 digital, IKA, Germany). After this, colloidal silica was added to the suspension under stirring and homogenized for 10 min (Fig. 2A). Following, using a peristaltic pump (Masterflex® L/S Easy-Load® II 77201-60, USA, Fig. 2B), the suspension was dripped in a 0.1 M  $\text{Ca}(\text{NO}_3)_2$  coagulating bath (Fig. 2C), remaining during 24 h to complete coagulation (Fig. 2D) [22,29]. After this period, the samples were washed with water and ethyl alcohol 70 % and dried at 60 °C for 24 h (Venticell, MMM Group, Germany) (Fig. 2D). Macrospheres were thermally treated at a  $5^\circ \text{C} \cdot \text{min}^{-1}$  heating rate up to 1500 °C for 3 h (Lindberg Blue M, Thermo Fisher Scientific, USA).

### 2.3. Physicochemical characterization

The total porosity was evaluated by mercury intrusion porosimeter (PoreSizer 9320, Micrometrics) and Archimedes' Principle according to ASTM B962-23 “Test Methods for Density of Compacted or Sintered Powder Metallurgy (PM) Products Using Archimedes Principle” [48]. The dry mass ( $M_d$ ) was determined by weighing samples after drying for 24 h at 60 °C, for apparent mass ( $M_{ap}$ ), the samples were submerged in water at room temperature for 24 h to fill the pores and then weighed submerged on distilled water; the humid mass ( $M_h$ ) was determined removing excess liquid from the sample's surface and then weighing once more. The water density was obtained from the table of density as a function of temperature.

Density ( $\rho$ ), relative density ( $\rho_r$ ), and total porosity ( $P$ ) were calculated by Eqs. (1)–(3), respectively:

$$\rho = M_d / ((M_h - M_{ap}) \times \rho_{\text{H}_2\text{O}}) \quad (1)$$

$$\rho_r = 100 \times (\rho / \rho_{\text{sol}}) \quad (2)$$

$$P = 100 - \rho_r \quad (3)$$

The solid density ( $\rho_{\text{sol}}$ ) was measured using a helium pycnometer (Ultrapyc 1200e, Quantachrome Instruments, USA) with ground powder samples.

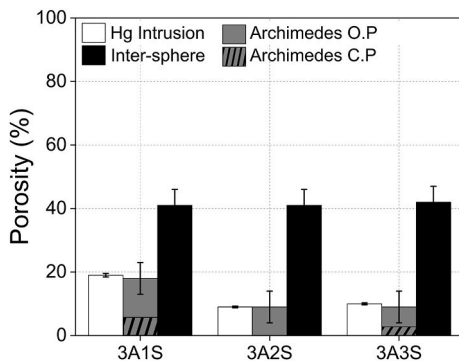
The bulk density was determined by the ratio of mass and volume of spheres in a graduated cylinder (Uniglas 185.010,  $10 \pm 0.2$  mL, Brazil); the apparent geometric density (AGD) was attained by the ratio of mass and volume of each sphere according to Eq. (4), and inter-sphere porosity by Eq. (5):

$$\text{AGD} = m / (4 / 3 \times \pi \times r_1 \times r_2 \times r_3) \quad (4)$$

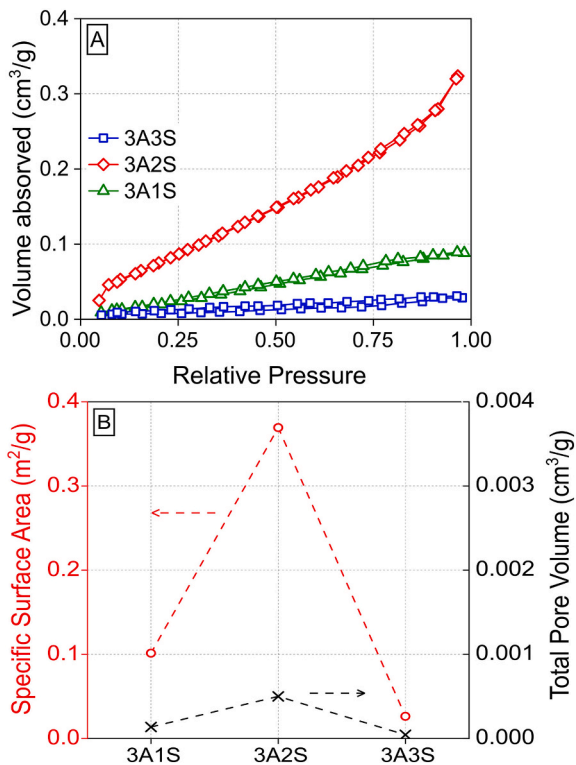
$$\text{Inter-sphere porosity} = 100 \times (1 - (\text{bulk density} / \text{AGD})) \quad (5)$$

Where  $r_1$ ,  $r_2$ , and  $r_3$  are the sphere radii on three different axes. The AGD was obtained by averaging ten measurements.

For the specific surface area (SSA,  $\text{m}^2 \cdot \text{g}^{-1}$ ), and total pore volume



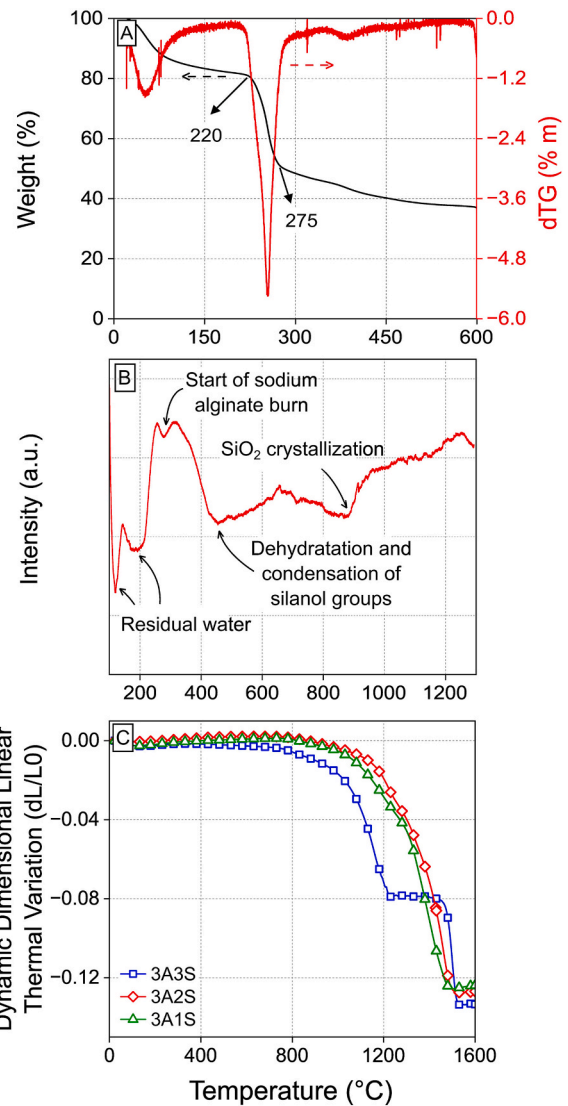
**Fig. 3.** – Total and inter-sphere porosity of alumina-silica macrosphere. White bars correspond to the intra-sphere porosity obtained by mercury intrusion porosimetry, grey bars represent the open intra-sphere porosity (O.P.) determined by Archimedes' Principle, dashed grey bars represent the close intra-sphere porosity (C.P.) determined by Archimedes' Principle, and black bars indicate the inter-sphere porosity. Data are presented as mean  $\pm$  standard deviation.



**Fig. 4.** – Nitrogen adsorption-desorption characterization of the alumina-silica macrosphere (A) Adsorption-desorption isotherms (BET method, 3A3S: blue  $\square$ , 3A2S: red  $\diamond$ , 3A1S: green  $\Delta$ ). (B) Specific surface area (BET method, red  $\circ$ , left axis) and total pore volume (calculated at  $P/P_0 \approx 0.99$ , black  $\times$ , right axis).

(TPV, cm<sup>3</sup>·g<sup>-1</sup>), the spheres were degassed for 2 h at 200 °C and measured by high-purity N<sub>2</sub> adsorption-desorption (BET method, NOVA 1200e, Quantachrome Instruments, USA) according to ASTM C 1069–09 “Standard Test Method for Specific Surface Area of Alumina or Quartz by Nitrogen Adsorption” [46].

Thermogravimetry analysis (TGA, Pyris 1, PerkinElmer, USA) was achieved on sodium alginate spheres at 600 °C, 5 °C·min<sup>-1</sup> heating rate under an air atmosphere flowing at 20 mL min<sup>-1</sup>, to evaluate polymer degradation. Differential scanning calorimetry (DSC, 404 F1, Netzsch, Germany) of the dry alumina/colloidal silica/SA macrospheres on the stoichiometric mullite composition (3A2S) was performed from room



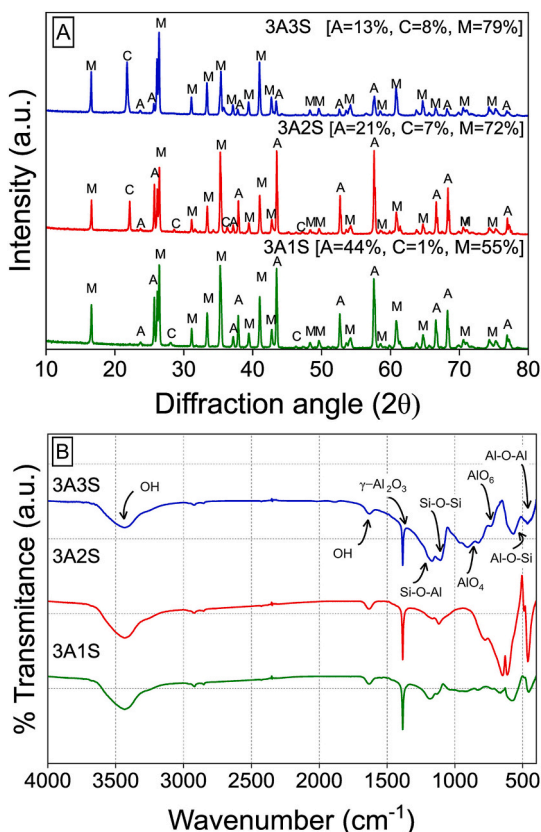
**Fig. 5.** – (A) Thermogravimetric analysis of sodium alginate sphere showing the mass loss profile during heating. (B) DSC of mullite macrosphere (3A2S) highlighting the thermal transitions of the composite system. (C) Dynamic linear shrinkage curves for the different compositions. Symbols: 3A3S: blue  $\square$ , 3A2S: red  $\diamond$ , 3A1S: green  $\Delta$ .

temperature up to 1350 °C at a rate of 10 °C·min<sup>-1</sup>. Dilatometric analysis (DIL402C, Netzsch, Germany) was conducted on green samples at 1600 °C for 3 h at a rate of 5 °C·min<sup>-1</sup>. Spheres were ground and uniaxially pressed to produce cylindrical samples measuring 6 mm in diameter and 8 mm in length.

Identification of crystalline phases was carried out by X-ray Diffraction (XRD, Rotaflex RV 200B, Rigaku-Denki Corp.), with Cu K $\alpha$  radiation ( $\lambda = 0.14506$  nm), diffraction angle ( $2\theta$ ) scanned between 10° and 80°, rate of 5°·min<sup>-1</sup>, step of 0.02°·s<sup>-1</sup>, current intensity 30 mA and voltage 40 kV, using powder samples obtained by grinding. For Fourier-transformed infrared spectroscopy (FTIR, PerkinElmer Frontier spectrometer, USA), spheres were ground and analyzed by the KBr pellet technique in the spectral range region from 400 to 4000 cm<sup>-1</sup>, with a 4 cm<sup>-1</sup> resolution and 36 scans per sample.

#### 2.4. Morphological properties

The morphology of the sintered samples was analyzed by scanning electron microscopy (SEM, Hitachi SU3800, Japan) at an accelerating



**Fig. 6.** (A) XRD diffractograms. Symbols: A:  $\text{Al}_2\text{O}_3$  (Corundum, JPCDS 1–1243), C:  $\text{SiO}_2$  (Cristobalite, JPCDS 1438), M:  $\text{Al}_6\text{Si}_2\text{O}_9$  (Mullite, JPCDS 1–163), 3A3S: blue line, 3A2S: red line, 3A1S: green line. (B) FTIR spectra of the alumina-silica macro-spheres sintered at  $1500^\circ\text{C}$ .

voltage of 15 kV. The samples were fixed in carbon tape with a thin layer of graphite conductive adhesive and sputter-coated (Cressington Sputter Coater, 108 Auto, USA) with an Au/Pd alloy conductive film for 1 min. ImageJ software was used to evaluate the range of diameter, circularity, and roundness [21].

## 2.5. Mechanical characterization

Vickers microhardness was measured on polished cross-section by the indentation technique (Microhardness Tester VMHT MOT, Leica, Germany), according to ASTM C 1327-99 “Standard Test Method for Vickers Indentation Hardness of Advanced Ceramics” [49] with a diamond pyramid indenter applying 100 g for 15 s. For this, macro-spheres were embedded in an unsaturated polyester resin, sanded and polished with successively finer grades of SiC sandpaper (#120, #320, #400, #600, #1200). The hardness results were the average of 10 measurements in different spheres.

The compression strength was measured in a universal testing machine (Model WDW-30E, 5 kN load cell,  $0.5\text{ mm min}^{-1}$  crosshead speed, adapted from ISO 13503 [50]). For this, 1 g of spheres was compressed into a cylindrical matrix ( $d_m = 15\text{ mm}$ ) at 30, 60, 80, 100, and 120 MPa. Each measurement was replicated 3 times. The compressive stress was calculated using Eq. (6). After each compression, the samples were sifted, the uncrushed samples were weighed, and the mechanical behavior was determined from the mass loss according to Eq. (7).

$$F = \pi \times \sigma \times d_m^2 / 4 \quad (6)$$

$$\text{Mass loss in compression} = (m_i - m_f) / m_i \times 100 \quad (7)$$

Where F is the strength,  $\sigma$  is the compressive stress,  $d_m$  is the matrix

diameter,  $m_i$  = mass of the samples before the mechanical test, and  $m_f$  = mass of uncrushed samples after the mechanical test.

Friability was studied as described by Coelho et al. (2019) [51]. For this, 2 g of macro-spheres were placed in a rotating drum (SOTAX/F1, Sotax Group, Germany), operating at 25 rpm for three cycles of 4 min each. After each cycle, the macro-spheres were collected, weighed, and the results were presented as mass loss, according to Eq. (7).

## 2.6. In vitro cytocompatibility

Cellular cytotoxicity was evaluated according to ISO 10993-5 “Biological evaluation of medical devices – Part 5: Tests for *in vitro* cytotoxicity” [52] testing the macro-spheres extracts. MC3T3-E1 pre-osteoblastic cells (CRL-2593, ATCC - Gibco) derived from mouse calvaria were cultured in alpha minimum essential medium ( $\alpha$ -MEM) (Sigma-Aldrich) supplemented with 10 % (v/v) fetal bovine serum (FBS, Gibco) and 1 % (v/v) penicillin-streptomycin (p/s, Sigma-Aldrich) at  $37^\circ\text{C}$  and 5 %  $\text{CO}_2$ . Cells were seeded on 96-well plates at a density of  $1 \times 10^5\text{ cells mL}^{-1}$  and incubated for 24 h at  $37^\circ\text{C}$ . The sample extracts were prepared according to ISO 10993-12 “Biological evaluation of medical devices - Part 12: Sample preparation and reference materials” [53]. The working volume was set at 100  $\mu\text{L}$ . Macro-spheres were sterilized by autoclaving at  $120^\circ\text{C}$  for 20 min, then immersed in supplemented  $\alpha$ -MEM with a fixed mass ratio to medium ( $0.2\text{ g mL}^{-1}$ ) and incubated at  $37^\circ\text{C}$  for 24 h and 5 %  $\text{CO}_2$ .

Cell metabolic activity was measured using the resazurin assay. The cell culture medium was removed, macro-sphere extracts were centrifuged for 10 s, added to the cell culture, and incubated for 24 h at  $37^\circ\text{C}$  and 5 %  $\text{CO}_2$ . The cytotoxic positive control was 1 % (v/v) Triton X-100 (Sigma-Aldrich), while only cells in  $\alpha$ -MEM were used as the negative control. Without seeding, the blanks were only composed of the samples’ extracts (or culture medium or 1 % (v/v) Triton for negative and positive controls, respectively). After 24, 48, and 72 h of incubation, the culture medium was discarded, and 10 % resazurin (v/v) in supplemented  $\alpha$ -MEM was added to each well and incubated for 3 h at  $37^\circ\text{C}$  and 5 %  $\text{CO}_2$ . After incubation, fluorescence was measured at 530 nm excitation and 590 nm emission in a Synergy MX fluorimeter (BioTek). Data were normalized relative to the negative control. Five samples per group were used in three independent assays.

The Live/Dead cell assay was also performed to evaluate cell viability by simultaneously quantifying live and dead cells. The live cells were stained with green-fluorescent calcein-AM (Thermo-Fisher), while dead cells were stained with red-fluorescent propidium iodide (PI - BD Biosciences). The cells were incubated with the sample extracts for one and three days at  $37^\circ\text{C}$  and 5 %  $\text{CO}_2$ . The positive and negative controls consisted of cells incubated with 1 % (v/v) Triton X-100 with supplemented  $\alpha$ -MEM, respectively. For each time point, culture medium was removed, 50  $\mu\text{L}$  of calcein diluted in  $\alpha$ -MEM ( $2\text{ }\mu\text{L mL}^{-1}$ ), and 50  $\mu\text{L}$  of PI diluted in phosphate buffer solution (PBS, 50 %v/v) were added to each well and then incubated for 30 min at  $37^\circ\text{C}$  and 5 %  $\text{CO}_2$ . After incubation, cells were visualized using an inverted fluorescence microscope (IFM, Zeiss, Germany) with green (488 nm) and red (594 nm) filters, and the acquired images were processed with ImageJ version 1.54 m.

## 2.7. Hemocompatibility

To assess the hemolytic potential of the macro-spheres, sterilized samples ( $2\text{ g mL}^{-1}$ ) by autoclave were incubated with human red blood cells (RBCs) according to ASTM F756:2017 “Standard Practice for Assessment of Hemolytic Properties of Materials” [54] and as described elsewhere [55]. Briefly, RBCs were extracted from human buffy coats (ethics protocol ref. [90]/19 with Hospital de São João, Porto, Portugal) by differential centrifugations at 400 G for 30 min. The upper layer was discarded, and the pellet (containing the RBCs) was diluted in PBS (1:400). The samples were incubated with isolated RBCs ( $4 \times 10^8\text{ cells mL}^{-1}$ ) in a 48-well plate and incubated for 3 h at  $37^\circ\text{C}$ . In addition, the

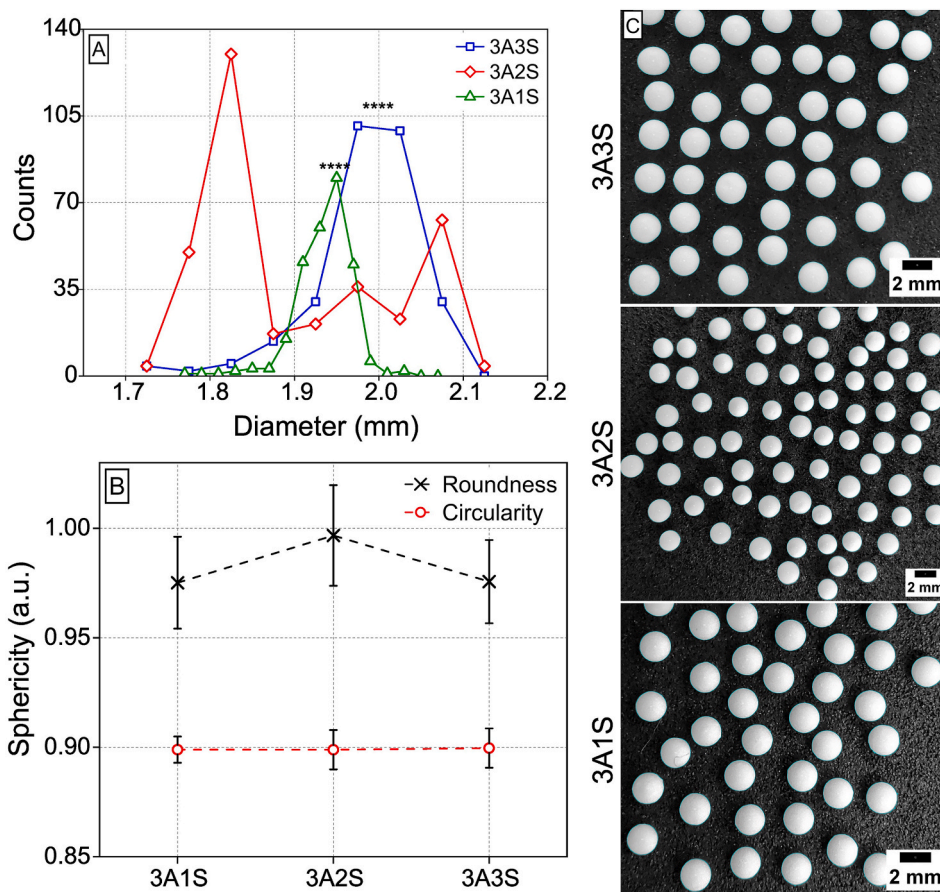


Fig. 7. (A) Particle size distribution. Symbols: 3A3S: blue  $\square$ , 3A2S: red  $\diamond$ , 3A1S: green  $\Delta$ ; (B) Sphericity parameters. Symbols: Roundness: black  $\times$ , Circularity: red  $\circ$ . Data are expressed as mean  $\pm$  SD. Significant values\*\*\*\*p < 0.0001 compared to 3A2S. (C) Original macrographs used in ImageJ analysis.

positive control (100 % hemolysis of RBCs) consisted of 1 % (v/v) Triton X-100 with RBCs, while the negative control was PBS mixed with RBCs. Following, the plate was centrifuged at 4000 rpm for 15 min, and 100  $\mu$ L of the supernatant was collected for a 96-well plate to read the absorbance at 380, 415, and 450 nm using the SynergyMiX fluorimeter (BioTek). The amount of hemoglobin (HB) was calculated as the following Eq. (8):

$$\text{HB (mg.dL}^{-1}\text{)} = ((2 \times A_{415} - (A_{380} + A_{450})) \times 100) / E \quad (8)$$

A415, A380, and A450 represent the absorbance read at 415 nm, 380 nm, and 450 nm, respectively; E is the molar absorptivity of oxyhemoglobin at 450 nm.

The hemolytic potential is determined by Eq. (9):

$$\text{Hemolysis (\%)} = \text{RH}_{\text{sample}} / \text{RH}_{\text{total}} \quad (9)$$

Where RH<sub>total</sub> is the amount of hemoglobin released in the positive control. Each assay was performed with five replicates.

## 2.8. In vitro proliferation

MC3T3-E1 Cells were cultured in  $\alpha$ -MEM supplemented with 10 % (v/v) FBS and 1 % (v/v) p/s and incubated at 37  $^{\circ}$ C and 5 % CO<sub>2</sub>. After cell confluence, cells were seeded on the macrospheres at  $6 \times 10^4$  cells.  $\text{cm}^{-2}$ , and incubated for 3, 7, and 14 days at 37  $^{\circ}$ C and 5 % CO<sub>2</sub>. Before seeding, samples were sterilized by autoclaving. Cells grown on the tissue culture plates (TCPS) without macrospheres were considered 100 % of cell viability or control [56].

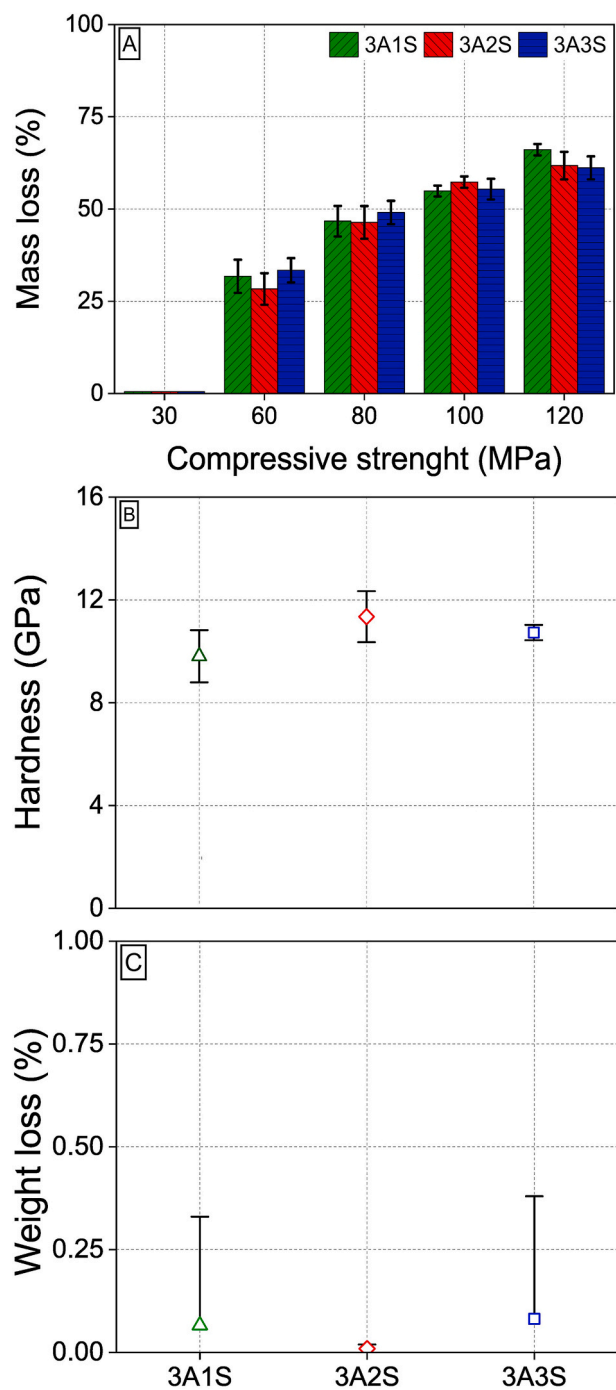
Cellular metabolic activity was evaluated using the resazurin assay. After each time point, the culture medium was removed, and 10 %

resazurin (v/v) was added to each well and incubated for 4 h. After incubation, the fluorescence was measured at an excitation of 530 and emission of 590 nm wavelengths in a SynergyMX fluorimeter (BioTek). Afterwards, the wells were cleaned with sterile PBS and loaded with fresh supplemented  $\alpha$ -MEM. This test was performed using five samples ( $2 \text{ g mL}^{-1}$ ) for each macrosphere group in three independent assays. The results were expressed as relative fluorescent units (RFU). Furthermore, this assay was also performed using an osteogenic medium composed of supplemented  $\alpha$ -MEM medium with 10 mM  $\beta$ -glycerophosphate, 0.01  $\text{mg mL}^{-1}$  l-ascorbic acid, and  $10^{-8}$  M dexamethasone.

The cultured samples were analyzed by confocal laser scanning microscopy (CLSM) and scanning electron microscopy (SEM) to observe cell morphology and adherence to the sample surfaces.

After 14 days of cell culture, the medium was discarded, and the samples were rinsed in non-sterile PBS. The samples were fixed with 4 % paraformaldehyde (Sigma-Aldrich) for 30 min, followed by incubation in 0.2 % (v/v) Triton X-100 solution (Sigma-Aldrich) for 10 min and 1 % (w/v) bovine serum albumin (BSA, Sigma-Aldrich) for 10 min. Cell cytoskeleton filamentous actin (F-actin) was stained with Alexa Fluor conjugated phalloidin 488 in 1 % BSA solution for 20 min at 50 rpm. Samples were washed twice with PBS, and nuclei were stained with DAPI (4',6-diamidino-2-phenylindole) ( $0.5 \mu\text{g mL}^{-1}$ ) for 20 min at 50 rpm. Samples were washed twice with PBS, and images of fluorescent-labeled cells were obtained using a confocal laser scanning microscope CLSM (TCS-SP5 AOBS, Leica microsystems) using 405 and 594 nm excitation lasers.

For SEM analysis, samples were fixed in 1.5 % (v/v) glutaraldehyde (diluted in 25 % cacodylate solution) for 15 min, followed by sequential dehydration in graded ethanol solutions (50 %, 70 %, 90 % and 100 % v/v) and hexamethyldisilane: ethanol (50 %, 70 %, 90 % and 100 % v/v,



**Fig. 8.** Mechanical properties of alumina-silica macrospheres. Symbols 3A1S: green  $\Delta$ , 3A2S: red  $\diamond$ , 3A3S: blue  $\square$ . (A) Mass loss (%) as a function of compressive strength (MPa). (B) Vickers microhardness (GPa). All samples presented high hardness, with slightly higher values for the 3A2S composition. (C) Mass loss (%) after friability test. Data are expressed as mean  $\pm$  SD.

HMDS, Sigma-Aldrich) series. The samples were sputter-coated (Cresington Sputter Coater, 108 auto) with a 10 nm Au/Pd film for 1 min and observed by SEM (Nova NanoSEM 200 microscope, FEI), at 10 kV in SE mode.

### 2.9. Statistical analysis

All statistical analyses were performed using a One-Way analysis of variance (ANOVA) with GraphPad Prism version 5.02. Results are presented as mean  $\pm$  standard deviation. Statistically significant differences

were indicated with \* $p < 0.05$ , \*\* $p < 0.01$  and \*\*\*\* $p < 0.0001$ .

## 3. Results and discussion

### 3.1. Physicochemical characterization

The porosity results (Fig. 3) indicated low intra-sphere porosity (>20 %) in all compositions. The reduction in porosity with increasing colloidal silica content can be explained by improved packing as colloidal particles fill gaps that micrometric particles cannot reach [57, 58], as observed in studies combining colloidal silica with other materials, such as MgO [59]. Furthermore, despite the low intra-sphere porosity (>20 %), due to their loose-fill format, high levels of inter-sphere porosity (40 %) can be achieved in all compositions, suggesting that the inter-sphere porosity was not directly related to the final composition of the synthesized compound or phases present ( $\text{Al}_2\text{O}_3/\text{Al}_6\text{Si}_4\text{O}_{13}/\text{SiO}_2$ ). The advantages of using porous implants include enhanced nutrient transport, vascularization, and cell migration, as well as an increased contact area between the implant and the bone, which together contribute to improved osseointegration [2,5,60, 61].

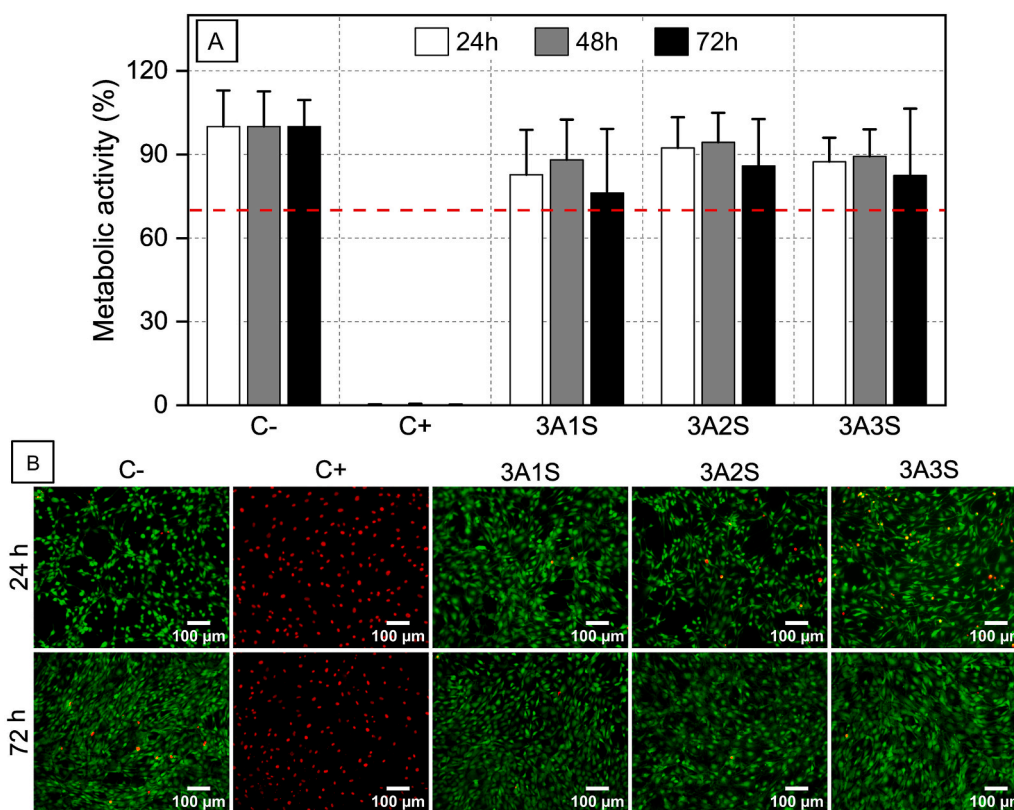
Porosity is a critical characteristic for cell adhesion and proliferation. The growth of osteoblastic cells has been reported in scaffolds with pore sizes ranging from 50 to 200  $\mu\text{m}$  [62]–400  $\mu\text{m}$  [63], and up to 600  $\mu\text{m}$  [64], where nutrient transport is more effective in promoting metabolic activity and cell proliferation within macropores. In addition, the low fraction of closed porosity obtained by Archimedes' method indicates that most pore volume is accessible, thereby favoring an open pore network that supports fluid transport and nutrient diffusion, increasing the contact area between the implant and the bone, which is essential for cell migration and proliferation within the implant [36,61,65,66]. The ability to tailor intra-sphere porosity without compromising inter-sphere architecture represents a promising strategy for multi-functional design.

The type II typical  $\text{N}_2$  adsorption isotherm (Fig. 4A) is typically observed in a non-porous or macroporous structure [67].  $\text{N}_2$  adsorption increased at high pressure, and when the adsorption and desorption curves do not coincide, hysteresis could occur during desorption [44], mainly in the case of aggregates with slit-shaped pores [67]. The 3A2S sample, in addition to higher specific surface area and total pore volume (Fig. 4B), showed a high absorbed volume, indicating a more open structure and greater pore accessibility. These results could suggest greater biological activity in this sample compared to 3A1S and 3A3S.

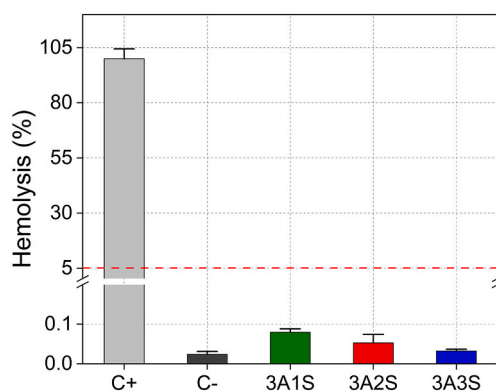
Thermogravimetric analysis (TGA) of the sodium alginate (SA) sphere is represented in Fig. 5A, showing the mass loss profile during heating. The initial weight loss below 150  $^\circ\text{C}$  is associated with the removal of physically adsorbed water [68]. The major mass-loss event between 200 and 300  $^\circ\text{C}$  corresponds to the thermal degradation of the sodium alginate [68,69].

DSC results revealed the reactions and phase transformations occurring during thermal treatment (Fig. 5B). An endothermic peak at 120  $^\circ\text{C}$  could be associated with the release of residual water, the burning of SA at 278  $^\circ\text{C}$  [70,71]. In line with the TGA results (Fig. 5A), the peak around 450  $^\circ\text{C}$  may be related to the dehydration and condensation of the silanol groups (forming Si–O–Si bonds and releasing water) [72] and the crystallization of  $\text{SiO}_2$  can be associated with the 875  $^\circ\text{C}$  peak [73,74].

Dilatometric analysis (Fig. 5C) showed that all samples exhibit thermal shrinkage above 1200  $^\circ\text{C}$ , with shrinkage intensity varying according to silica content. Furthermore, the densification of the 3A3S sample at lower temperatures, possibly due to the glass transition temperature of  $\text{SiO}_2$  ( $T_g$ , approximately 698  $^\circ\text{C}$ ) [75–77], when particles became soft and deformable, or due to the formation of cristobalite at lower temperatures than mullite or  $\text{Al}_2\text{O}_3$  sintering [74,78–81]. In all conditions, the differential thermal linear variation was interrupted around 1500  $^\circ\text{C}$ . It is known that the densification of mullite ceramics



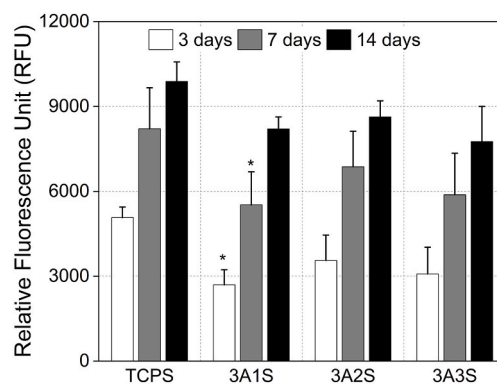
**Fig. 9.** Cell viability of MC3T3-E1 cells. (A) Metabolic activity over time with the sample extracts for different groups: C<sup>-</sup> (negative control), C<sup>+</sup> (positive control), 3A1S, 3A2S, 3A3S (experimental samples); red dashed line indicates 70 % cell viability according to ISO 10993. White bars correspond to 24 h, grey bars to 48 h, and black bars to 72 h of incubation. Data are expressed as mean ± SD. (B) Live/Dead cell viability staining after 24 and 72 h. The color green corresponds to living cells (stained with calcein) and the color red to dead cells (stained with propidium iodide). Scale bar: 100 μm.



**Fig. 10.** Hemolysis activity of alumina-silica microspheres after exposure to red blood cells. C<sup>+</sup> (positive control, LT grey bar): 1 % Triton; C<sup>-</sup> (negative control, grey bar): PBS; 3A1S (green bar), 3A2S (red bar), 3A3S (blue bar): experimental samples. The red dashed line at 5 % indicates hemocompatibility according to ASTM F756:2017 standard. Data are expressed as mean ± SD.

occurs at temperatures around 1600 °C [82,83] by a liquid phase formation; however, the use of colloidal precursors, as colloidal silica, can decrease the sintering temperature [44,84].

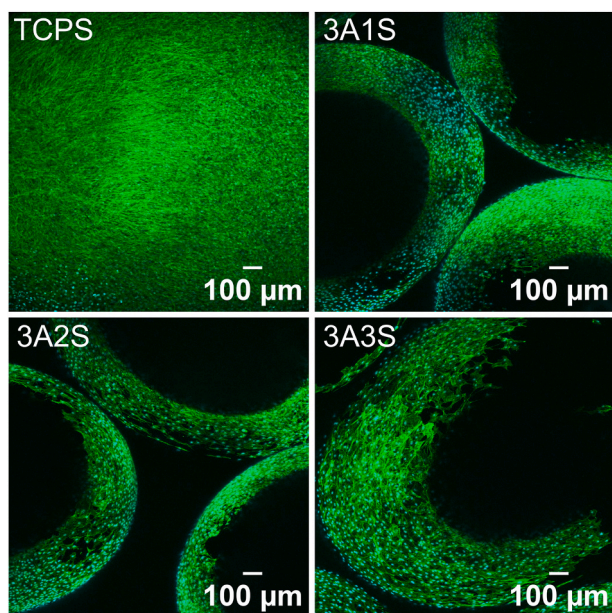
The phase composition of the alumina-silica microspheres sintered at 1500 °C is represented in Fig. 6A. In the XRD diffractograms of the sintered samples the identified phases corresponded to alumina (A, JPCDS 1–1243), cristobalite (C, JPCDS 1–438), and mullite (M, JPCDS 1–163). The mullite *in situ* is reported at lower temperatures for systems with other SiO<sub>2</sub> sources [82,84,85]. However, cristobalite formation can occur at low temperatures [74,86], consuming the SiO<sub>2</sub> available to



**Fig. 11.** Cell metabolic activity of MC3T3 cultured on alumina-silica microspheres over a 14-day culture period. TCPS (control): PBS; 3A1S, 3A2S, 3A3S: experimental compositions. White bars correspond to 3, grey bars to 7, and black bars to 14 days of incubation. An increase in fluorescence intensity over time indicates progressive cell adhesion and proliferation on all compositions. Data are expressed as mean ± SD. \*p ≤ 0.05 comparing to 3A2S.

react with Al<sub>2</sub>O<sub>3</sub> at higher temperatures. This may have contributed to the simultaneous production of the three phases. The biocompatibility of all these phases supports the potential use of these samples in biomedical implants [27,42,43].

The FTIR spectra (Fig. 6B) analysis confirmed the formation of aluminosilicate structures, consistent with mullite development. In more detail, the bands referred to stretching and bending of adsorbed water and hydroxyl groups were identified at 3420 and 1632 cm<sup>-1</sup> [87–89]. The peaks at 1170 and 648 cm<sup>-1</sup> correspond to Si–O–Al [87],



**Fig. 12.** Cell adhesion on the surface of the TCPS, 3A1S, 3A2S, 3A3S after 14 days. The color green corresponds to cell cytoskeleton actin (stained with Alexa Fluor and phalloidin), and the color blue corresponds to cell nuclei (stained with DAPI). The green fluorescence signal indicates viable adherent cells, demonstrating successful cell attachment and spreading. Scale bar: 100  $\mu\text{m}$ .

and at  $1110\text{ cm}^{-1}$  to the asymmetric stretch of Si–O–Si of the  $\text{SiO}_2$  [88,90]. The band at  $1385\text{ cm}^{-1}$  has been identified as Al–O bonds in  $\text{Al}_2\text{O}_3$  [89], at  $825$  and  $735\text{ cm}^{-1}$  as tetrahedral Al–O [38]. Finally, the peaks at  $570$  and  $468\text{ cm}^{-1}$  were attributed to Al–O vibration modes resulting from  $\text{AlO}_6$  mullite groups [88,90].

The silanol groups (Figs. 5B and 6B) are essential for hydroxyapatite nucleation in contact with body fluids, thereby forming a bioactive layer on the biomaterial surface that mimics the mineral composition of human bone [31,91–93]. This layer will promote an integration between the implant and native bone, providing an interface that stimulates bone regeneration [91,94–96]. Furthermore, Si–OH acts directly on the absorption of proteins by cells, which can promote their proliferation and differentiation [97,98], thus improving mineralization, new bone formation, and contributing to implant regeneration and integration [99,100].

### 3.2. Morphological properties

The particle size distribution (Fig. 7A) and sphericity (roundness and circularity, Fig. 7B) of alumina-silica macrospheres were determined by ImageJ analysis from the corresponding macrographs (Fig. 7C). There was a wide range in diameter distribution after sintering, particularly for the 3A2S condition (Fig. 7A), which was reduced for the 3A1S and 3A3S compositions. This distribution has been observed in studies of bioglass spheres produced by the same technique [21]. Comparing the average diameters obtained in the 3A2S sample with those in the others, it was found that the 3A2S sample was statistically different. This may have occurred due to the difference in the production of the cristobalite and mullite phases at high temperatures (Fig. 6). Obtaining mullite *in situ* generally has an expansive character due to its low solid density ( $3.2\text{ g cm}^{-3}$ ) compared to alumina ( $4.0\text{ g cm}^{-3}$ ), and the shrinkage or densification is improved [101,102] with the increase in the amount of  $\text{SiO}_2$  available in the system (Fig. 5C). The sphericity values range from 0.00 to 1.00, with 1.00 indicating a perfect sphere. Sphericity was assessed by circularity and roundness (Fig. 7B), and the samples did not show statistical differences, as all samples exhibited a circularity of approximately  $0.90 \pm 0.02$  and roundness ranging from 0.97 to 0.99, indicating

their nearly perfect sphericity. Alumina spheres fabricated by the same technique presented similar sphericity [103]. Optimal sphericity values improve packing, generating an interconnected macroporosity between spheres that could support nutrient transport and cell growth across the implant [21,25].

### 3.3. Mechanical characterization

The compressive strength of the spheres was evaluated by their resistance to mass loss under increasing mechanical stress. At 30 MPa, all formulations retained complete structural integrity, with zero mass loss observed (Fig. 8A). Mass loss increased as stress increased, reaching 70 % at 120 MPa. It is important to note that the compressive performance of the samples aligns with biological benchmarks: human cortical bone can withstand compressive strengths of 150 MPa, whereas cancellous bone supports around 20 MPa [27,100,104]. Therefore,  $\text{Al}_2\text{O}_3$ – $\text{SiO}_2$  spheres could be tailored for use at different anatomical sites, depending on the mechanical demands of the implantation site.

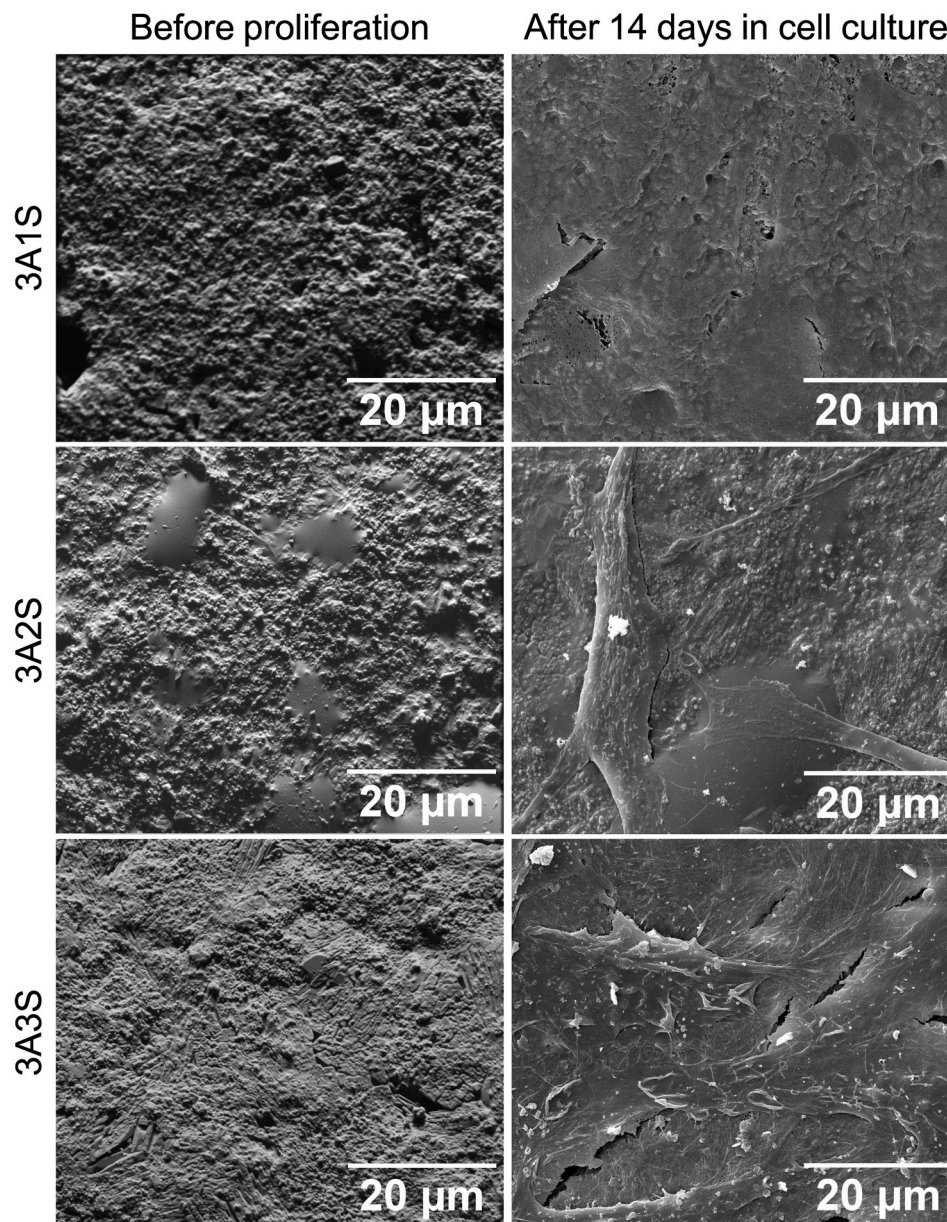
Vickers hardness testing is widely used for characterizing biomaterials due to its suitability for evaluating thin components and fine microstructures. This method can estimate the degree of mineralization and overall quality of bone tissue, which often varies depending on anatomical site and bone size [105,106]. Additionally, it enables direct comparison of the mechanical properties of synthetic materials with those of native bone tissue. In this study, all  $\text{Al}_2\text{O}_3$ – $\text{SiO}_2$  bioceramic spheres presented a hardness of approximately 10 GPa (Fig. 8B), with the 3A2S sample exhibiting the highest value, followed by 3A3S and 3A1S. These values are in agreement with previously reported data for mullite-based ceramics sintered at approximately  $1500\text{ }^\circ\text{C}$  [107,108]. The high hardness values observed here suggest that the materials are suitable for applications requiring wear resistance and mechanical durability. Additionally, the weight loss remained below 1 % for all samples (Fig. 8C), indicating good wear resistance in the loose-fill application.

### 3.4. *In vitro* cytocompatibility

Biocompatibility is a critical characteristic of macrospheres used as bone grafts, as it ensures that the material integrates with the body without causing adverse effects. According to the ISO 10993-5 standard [52], cell viability above 70 % is considered non-cytotoxic. The cytocompatibility of the experimental samples was assessed using a quantitative cell viability assay and qualitative live/dead cell imaging (Fig. 9). At all evaluated time points, negative control ( $\text{C}^-$ ) maintained high viability (>95 %), confirming normal cell growth (Fig. 9A). The positive control ( $\text{C}^+$ ) exhibited cytotoxicity, with viability below 1 %. The macrospheres were cytocompatible, exhibiting cell viability above 90 % under all tested conditions, even after 72 h of exposure (Fig. 9B), indicating that the materials do not induce cytotoxicity effects [25,56]. Although no significant deviations were observed, slight differences in cell viability were noted among 3A1S, 3A2S, and 3A3S, which may be attributed to variations in formulation and surface characteristics. Complementing this, samples showed no statistical differences compared to the  $\text{C}^-$ , indicating that the material did not inhibit cell activity, even with increasing incubation time. The Live/Dead images supported these findings, revealing a predominance of live cells across all experimental groups (Fig. 9B), exhibiting a similar behavior to the  $\text{C}^-$ . Furthermore, cell density increased with incubation time, showing that the material does not impede cell growth, as observed with biocompatible materials [51]. Given these results, the produced macrospheres showed promising biocompatibility for use in bone tissue engineering.

### 3.5. Hemocompatibility

The hemolytic potential of the materials was evaluated to assess their



**Fig. 13.** SEM micrographs of alumina-silica macrospheres before cell seeding (left) and after 21 days of MC3T3 culture (right). Post-culture images show adhered and spread cells with extracellular matrix formation across the surface. Scale bar: 20  $\mu\text{m}$ .

blood compatibility, which is critical for applications involving direct blood contact [55,109]. According to the ASTM F756:2017 standard [54], a material is considered non-hemolytic if hemolysis is below 5%. All experimental conditions demonstrated minimal hemolytic activity (<0.1%) (Fig. 10) and did not differ statistically from the  $\text{C}^+$  condition, indicating that the  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  macrospheres did not affect red blood cell integrity being classified as hemocompatible.

### 3.6. *In vitro* proliferation

To evaluate the *in vitro* cell proliferation, MC3T3-E3 cells were seeded on the microsphere samples and cultured for 14 days. At day 3, cell proliferation on all ceramic samples was lower than on the control (TCPS), although the differences were not statistically significant (Fig. 11). However, on day 7, a substantial increase in metabolic activity was observed across all groups, indicating that cell proliferation was not affected, even in direct contact with the material. Comparing the influence of the macrospheres' composition, a statistical difference was

only observed between the 3A2S and 3A1S conditions at the initial time (3 days), but this difference was not sustained after 14 days. Thus, the  $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  ratio in the composition of the macrospheres did not exert the most significant influence on metabolic activity with increasing incubation time.

Confocal laser scanning microscopy was used to qualitatively assess cell adhesion and spatial distribution on the surface after *in vitro* culture. The cells adhered to the entire surface of the spheres (Fig. 12). A higher cell density is observed in the contact area between the spheres, suggesting that tissue regeneration occurs primarily at the porosity between them.

The surface morphology of the samples was observed using scanning electron microscopy (SEM) before cell seeding and after 14 days of *in vitro* culture (Fig. 13). Before proliferation, all samples exhibited distinct microstructures. The 3A1S surface exhibited high roughness and open pores, which may initially improve cell attachment [110]. The 3A2S surface displayed a slightly smoother texture, which may facilitate initial cell anchorage [42]. In contrast, 3A3S showed a more textured

surface with elongated crystalline structures, potentially enhancing cell–material interaction. After 2 days of culture, all samples showed evidence of cellular attachment and extracellular matrix formation. In 3A1S, the surface appeared covered by a cellular layer, similar to that observed in other studies [25,36]. In 3A2S, a more defined cell morphology was observed, suggesting active interaction between cells and the substrate, and the 3A3S surface was extensively covered with a dense cellular layer and abundant osteoblastic-like structures, indicating robust cell proliferation [42,111,112].

#### 4. Conclusions

$\text{Al}_2\text{O}_3\text{-SiO}_2$  ceramic microspheres with different chemical compositions were produced by ionotropic gelcasting. Thermal treatment led to the formation of biologically favorable crystalline phases, including mullite and cristobalite. All compositions had good sphericity (circularity  $\sim 0.90$  and roundness  $\sim 0.97$ ), which allowed for easier packing and the formation of inter-sphere macroporosity ( $\sim 40\%$ ). The presence of silanol groups (Si–OH) can induce the formation of a bioactive surface, facilitating direct integration with native bone tissue, thereby enhancing osseointegration and stimulating osteoblastic activity. The mechanical properties, including high Vickers hardness ( $\sim 10$  GPa) and compressive resistance up to 120 MPa, meet the requirements of cancellous and some cortical bone regions, ensuring that the spheres can maintain structural integrity under physiological loads. *In vitro* biological evaluations confirmed the cytocompatibility and hemocompatibility of the material, as well as its ability to support cell adhesion, and proliferation. Among the three compositions, the stoichiometric mullite, sample 3A2S ( $3\text{Al}_2\text{O}_3\cdot 2\text{SiO}_2$ ), exhibited the most balanced combination of mechanical strength (improved compressive strength and hardness without excessive densification), specific surface area (more surface available for protein adsorption and cell interaction), and biocompatibility (good metabolic activity, cyto and hemocompatibility). Overall, these findings indicate that  $\text{Al}_2\text{O}_3\text{-SiO}_2$  microspheres combine structural, chemical, and biological properties that are synergistic with the demands of bone tissue regeneration. This supports their usage as injectable or granular materials for defect repair in orthopedic and dental applications.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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